



**UTHM**

Universiti Tun Hussein Onn Malaysia

**UNIVERSITI TUN HUSSEIN ONN MALAYSIA**

**FINAL EXAMINATION  
SEMESTER II  
SESSION 2016/2017**

COURSE : ROBOTIC SYSTEMS  
COURSE CODE : BEH41703  
PROGRAMME : BEJ  
EXAMINATION DATE : JUNE 2017  
DURATION : 3 HOURS  
INSTRUCTION : ANSWER ALL QUESTIONS

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THIS PAPER CONSISTS OF SIX (6) PAGES

**Q1** Consider the following cylindrical robot arm with one rotary joint and two prismatic joints in **Figure Q1**

- (a) Assign coordinate frames to the robot arm using the D-H algorithm. (5 marks)
- (b) Obtain a table of the D-H parameters of the robot. (5 marks)
- (c) Obtain the transformation matrices  $H_0^1$ ,  $H_1^2$  and  $H_2^3$  by using the D-H matrix as given below:

$$H_{i-1}^i = \begin{bmatrix} C\theta_i & -C\alpha_i S\theta_i & S\alpha_i S\theta_i & a_i C\theta_i \\ S\theta_i & C\alpha_i C\theta_i & -S\alpha_i S\theta_i & a_i S\theta_i \\ 0 & S\alpha_i & C\alpha_i & d_1 \\ 0 & 0 & 0 & 1 \end{bmatrix}$$

(5 marks)

- (d) Obtain the forward kinematics matrix  $H_0^3$ . (5 marks)

**Q2** **Figure Q2** shows a cylindrical arm with two prismatic joints and a rotary joint. The seven trigonometric equations and their solutions are given in **Table Q2**. The forward kinematic solution is given as below. Analyse the inverse position (joint angles) of the articulated arm from this forward kinematic,  $H_0^3$ .

$$H_0^3 = \begin{bmatrix} C_2 & 0 & -S_2 & -d_3 S_2 + a_2 C_2 \\ S_2 & 0 & C_2 & d_3 C_2 + a_2 S_2 \\ 0 & -1 & 0 & d_1 \\ 0 & 0 & 0 & 1 \end{bmatrix}$$



(20 marks)

- Q3** (a) Briefly discuss about the problem of singularity. (3 marks)
- (b) **Figure Q3 (b)** shows a spherical arm with two rotary joints and a prismatic joint. By applying the transformation matrix and arm parameters as in **Table Q3 (b)**, obtain the Jacobian matrix,  $J$ .

$$H_{i-1}^i = \begin{bmatrix} C\theta_i & -C\alpha_i S\theta_i & S\alpha_i S\theta_i & a_i C\theta_i \\ S\theta_i & C\alpha_i C\theta_i & -S\alpha_i S\theta_i & a_i S\theta_i \\ 0 & S\alpha_i & C\alpha_i & d_1 \\ 0 & 0 & 0 & 1 \end{bmatrix}$$

Jacobian matrix

$$\begin{bmatrix} v_x \\ v_y \\ v_z \\ \omega_x \\ \omega_y \\ \omega_z \end{bmatrix} = \begin{bmatrix} \frac{\partial f_1}{\partial q_1} & \frac{\partial f_1}{\partial q_2} & \frac{\partial f_1}{\partial q_3} \\ \frac{\partial f_2}{\partial q_1} & \frac{\partial f_2}{\partial q_2} & \frac{\partial f_2}{\partial q_3} \\ \frac{\partial f_3}{\partial q_1} & \frac{\partial f_3}{\partial q_2} & \frac{\partial f_3}{\partial q_3} \\ \eta_1 R_{3(3col)}^0 & \eta_2 R_{3(3col)}^1 & \eta_3 R_{3(3col)}^2 \end{bmatrix} \begin{bmatrix} \dot{q}_1 \\ \dot{q}_2 \\ \dot{q}_3 \\ \dot{q}_4 \\ \dot{q}_5 \\ \dot{q}_6 \end{bmatrix}$$

(17 marks)

**Q4** (a) From the perspective of robotics, list two (2) main reasons for using dynamics equations for robot modelling.

(2 marks)

(b) The links of an RP manipulator, shown in **Figure Q4**, have the following inertial tensors (relative to the frame with its origin positioned at the center of rotation  $\theta_1$ , with  $\theta_1$  being the rotation around z-axis):

$${}^o I_1 = \begin{bmatrix} I_{xx1} & 0 & 0 \\ 0 & I_{yy1} & 0 \\ 0 & 0 & I_{zz1} \end{bmatrix}$$

$${}^o I_2 = \begin{bmatrix} I_{xx2} & 0 & 0 \\ 0 & I_{yy2} & 0 \\ 0 & 0 & I_{zz2} \end{bmatrix}$$



and total mass of  $m_1$  and  $m_2$ . As shown in the Figure, the center of mass of link-1 is located at a distance of  $l_1$  from the joint-1 axis, and the center of mass of link-2 is at a variable distance of  $d_2$  from the joint-1 axis. Use Lagrangian dynamics to determine the equation of motion for the manipulator.

(18 marks)

- Q5** Consider a single-link robot manipulator with a rotary joint as shown in **Figure Q5**. The differential equation of the above single link robot manipulator given by

$$\left(I_m + \frac{I_l}{n^2}\right)\ddot{\theta}_m + \left(B_m + \frac{B_l}{n^2}\right)\dot{\theta}_m + \frac{mgl}{n}\sin\left(\frac{\theta_m}{n}\right) = u$$

- (a) Linearize the above differential equation with some assumptions. (5 marks)
- (b) Transform the linearized equation to the Laplace equation to formulate the transfer function  $\Theta_m(s)/U(s)$  (4 marks)
- (c) Draw the block diagram and label of the complete system with a PD controller. [Hint: The transfer function of a PD controller  $G(s) = K_p + K_D s$ ] (5 marks)
- (d) Obtain the transfer function for the PD controller with stable values of  $K_p$  and  $K_D$  [Hint: find out the *characteristic equation* of the closed loop system]. (6 marks)

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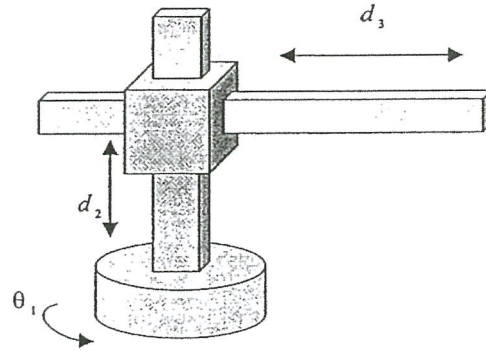


Figure Q1

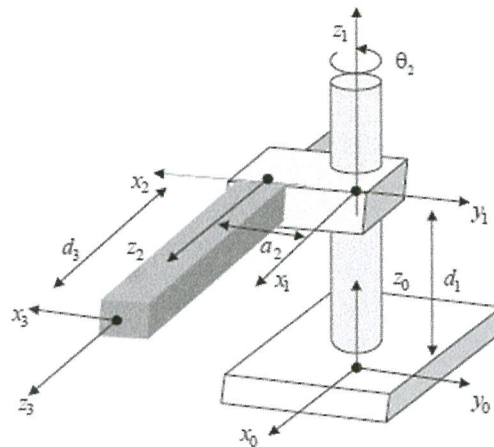


Figure Q2

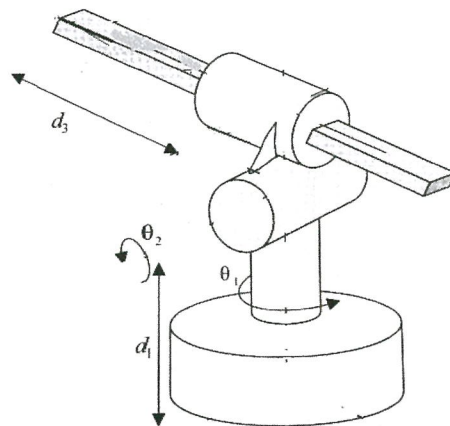
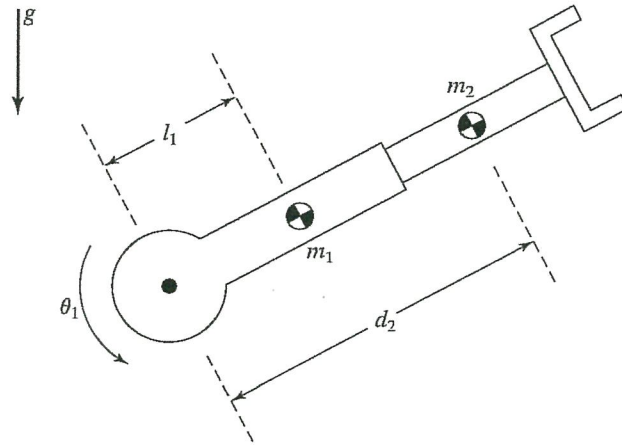


Figure Q3(b)

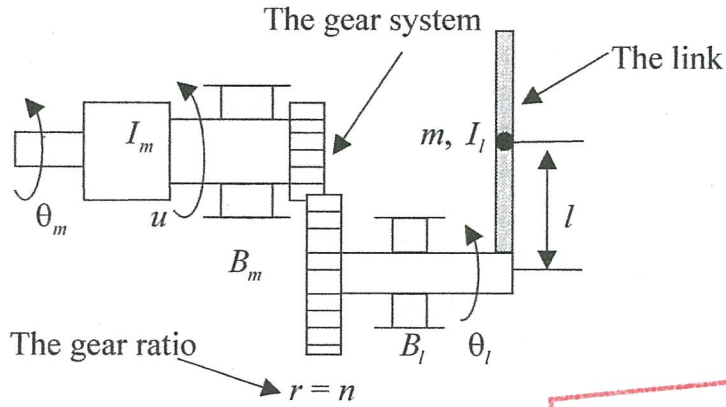
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**Table Q3 (b)**

Link	$\theta_i$	$a_i$	$\alpha_i$	$d_i$
1	$\theta_1$	0	$-90^\circ$	$d_1$
2	$\theta_2$	$a_2$	$-90^\circ$	0
3	0	0	0	$d_3$



**Figure Q4**



**Figure Q5**

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