



UNIVERSITI TUN HUSSEIN ONN MALAYSIA

FINAL EXAMINATION

SEMESTER II

SESSION 2016/2017

COURSE NAME : INSTRUMENTATION AND CONTROL SYSTEMS
COURSE CODE : BEH 22003
PROGRAMME CODE : BEJ
EXAMINATION DATE : JUNE 2017
DURATION : 3 HOURS
INSTRUCTION : ANSWER ALL QUESTIONS



THIS QUESTION PAPER CONSISTS OF **EIGHT (8)** PAGES

- Q1** (a) List down the advantages and disadvantages of the open loop control system. (3 marks)
- (b) Explain clearly how one of the disadvantages of the open loop control system that you have listed in question **Q1(a)** can occur in a practical control system. (7 marks)
- (c) List down the advantages and disadvantages of the closed loop control system. (3 marks)
- (d) Explain clearly how one of the advantages of the closed loop control system that you have listed in question **Q1(c)** can occur in a practical control system. (7 marks)

Q2 **Figure Q2** shows a schematic diagram for a field control direct current motor. Given that the motor torque $T_m(t)$ is proportional to the field current $i(t)$ i.e. $T_m(t) = K_f i(t)$ where K_f is the motor torque constant. The armature current I_a is assumed to be constant. J_m and B_m are the moment of inertia and the viscous frictional torque constants respectively referred to the motor shaft.

- (a) Determine the relevant equations for this system. (4 marks)
- (b) Build the block diagram for this system. (5 marks)
- (c) Obtain the transfer function of $\theta_m(s)/V(s)$ where $\theta_m(s)$ and $V(s)$ are the Laplace transformations of the angular position $\theta_m(t)$ and the motor voltage $v(t)$ respectively. (5 marks)
- (d) By using a suitable schematic diagram, design a closed-loop control system to control the angular position $\theta_m(t)$. (6 marks)

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Q3 (a) Describe the type of responses of a second order prototype closed loop control system that relates to the values of the damping ratio ζ .

(8 marks)

(b) **Figure Q3(b)** shows the block diagram of a control system where K_s and K_g are the amplifier gain and the tachometer constant respectively where $K_s = 100$ and $K_g = 0.11$.

(i) Determine the percentage maximum overshoot μ_p and the time this maximum overshoot to occur T_p .

(4 marks)

(ii) Obtain the unit step response $c(t)$, of this control system.

(6 marks)

(iii) Sketch the response $c(t)$ obtained in **Q3(b)(ii)**.

(2 marks)

Q4 (a) Describe the phenomenon that will occur in a control system when an off-on controller is being employed in the system.

(5 marks)

(b) Explain clearly why dead-zone or neutral zone is implemented in a off-controller.

(5 marks)

(c) The temperature of water in a tank is controlled by an on-off controller. When the heater is *off*, the temperature drops at 2°C per minute. When the heater is *on* the temperature rises at 4°C per minute. The setpoint or the input is 50°C and the neutral zone is $\pm 20\%$ of the setpoint. There is a 0.5 min lag at the *on* and *off* switch points.

(i) Plot the water temperature versus time.

(7 marks)

(ii) Determine the period of oscillation.

(3 marks)

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Q5 (a) Explain the difference between active and passive transducers.

(4 marks)

(b) A resistive potentiometer transducer with a shaft stroke of L cm is applied in the circuit of **Figure Q5**. The total resistance of the potentiometer is $R \Omega$, and the applied voltage is V_T V. The travel distance from the wiper to point B is x cm.

(i) By assuming that the transducer is linear, obtain the relationship between the output voltage V_o and the distance x .

(6 marks)

(ii) Given that $L = 12$ cm, $x = 3$ cm, $R = 10$ k Ω and $V_T = 10$ volts, calculate the voltage V_o .

(2 marks)

(iii) Propose a suitable method where this resistive transducer can be used to measure the bumpiness or the unevenness of a roadway.

(8 marks)

– END OF QUESTIONS –

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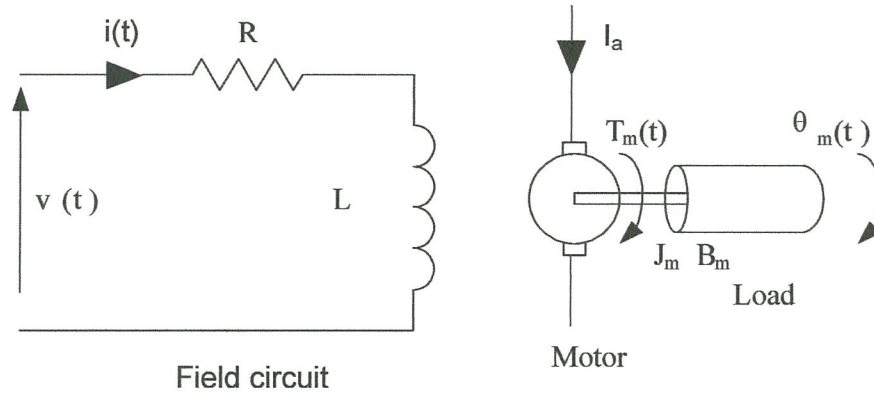


Figure Q2

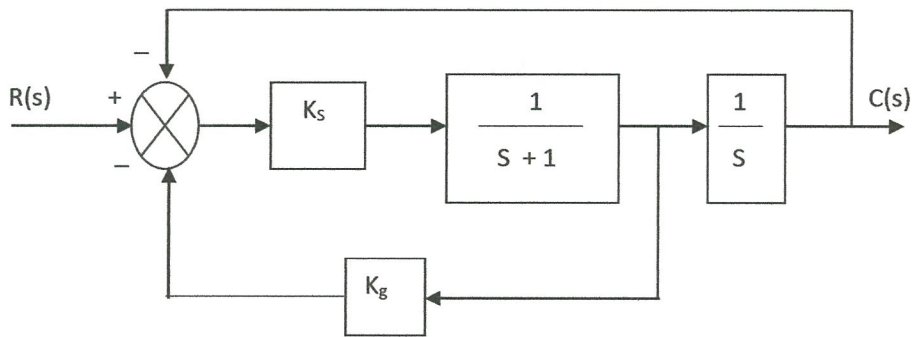


Figure Q3(b)

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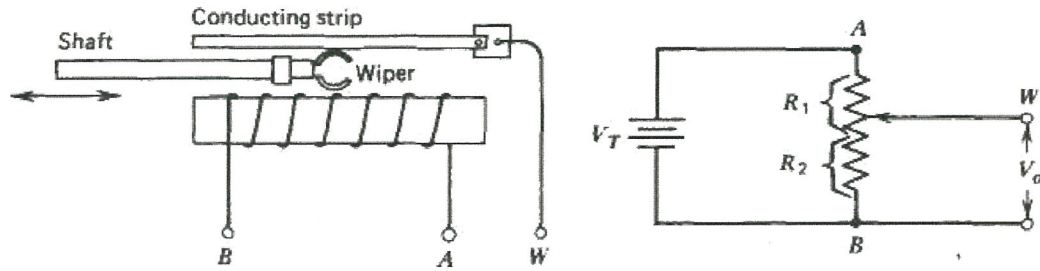


Figure Q5

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Table 1 : Laplace Transform Table

$f(t)$	$F(s)$
$\delta(t)$	1
$u(t)$	$\frac{1}{s}$
$tu(t)$	$\frac{1}{s^2}$
$t^n u(t)$	$\frac{n!}{s^{n+1}}$
$e^{-at}u(t)$	$\frac{1}{s+a}$
$\sin \omega t u(t)$	$\frac{\omega}{s^2 + \omega^2}$
$\cos \omega t u(t)$	$\frac{s}{s^2 + \omega^2}$
$\cos \omega t u(t)$	$\frac{s}{s^2 + \omega^2}$
$e^{-at} \cos \omega t u(t)$	$\frac{s+a}{(s+a)^2 + \omega^2}$
$e^{-at} \sin \omega t u(t)$	$\frac{\omega}{(s+a)^2 + \omega^2}$

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Table 2 : Second order prototype equations

$\frac{C(s)}{R(s)} = \frac{\omega_n^2}{s^2 + 2\zeta\omega_n s + \omega_n^2}$	$T_r = \frac{\pi - \cos^{-1} \zeta}{\omega_n \sqrt{1 - \zeta^2}}$
$\mu_p = e^{\frac{-\zeta\pi}{\sqrt{1 - \zeta^2}}}$	$T_p = \frac{\pi}{\omega_n \sqrt{1 - \zeta^2}}$
$T_s = \frac{4}{\zeta\omega_n} \text{ (2\% criterion)}$	$T_s = \frac{3}{\zeta\omega_n} \text{ (5\% criterion)}$

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