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UNIVERSITI TUN HUSSEIN ONN MALAYSIA

**FINAL EXAMINATION
SEMESTER I
SESSION 2016/2017**

COURSE NAME : ELECTRONIC CIRCUITS ANALYSIS
AND DESIGN

COURSE CODE : BEL 30403

PROGRAMME CODE : BEJ

EXAMINATION DATE : DECEMBER 2016 / JANUARY 2017

DURATION : 3 HOURS

INSTRUCTION : ANSWERS ALL QUESTIONS

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THIS QUESTION PAPER CONSISTS OF NINE (9) PAGES

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Q1 In October 2016, Jurutera Hati Suri Sdn Bhd has been awarded a project to design flood detector by Jabatan Pertahanan Awam Malaysia. To kickoff the project immediately, they plan to utilise operational amplifier as the fundamental component of their initial design.

- (a) In the first design, the detector circuit is designed such that it
- recognises as low as 0.8 V of input voltage for flood warning, and
 - produces 10 V when flood warning is activated, otherwise the output remains at -10 V

(i) Show a possible circuit design to satisfy the pre-defined outcomes mentioned in **Q1(a)**.

(4 marks)

(ii) Prove that, using input-output relationship diagram, the circuit design in **Q1(a)(i)** could achieve the prerequisite conditions mentioned in **Q1(a)**.

(6 marks)

(b) Next, the circuit in **Q1(a)** is modified such that the input voltage for flood warning is raised to Zener voltage of 1.2 V.

(i) Show a possible circuit design to satisfy the pre-defined outcomes mentioned in **Q1(b)**.

(4 marks)

(ii) Show the input-output waveform to prove that the circuit design in **Q1(b)(i)** could achieve condition mentioned in **Q1(b)**.

(6 marks)

Q2 In order to escalate competition in broadband services, the Malaysian Communications and Multimedia Commission (MCMC) has appointed Pening Lalat Sdn Bhd to operate 4G-LTE in a new band spectrum. The awarded spectrum is centred at 840 MHz with bandwidth of 20 MHz.

(a) As a leader of this project, design an active filter that could ensure that the transmitted signal will reach the end user within the specified band spectrum. The frequency response shall

- be maximally flat response,
- have roll-off not more than 20 dB/decade, and
- have gain not less than 50 dB.

(12 marks)

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- (b) Verify that the filter design in **Q2(a)** meets the requirement of your client, Pening Lalat Sdn Bhd in which you need to show:
- quality factor of filter, and
 - a complete frequency response.

(8 marks)

Q3 In order to improve mobile communication in Parit Raja, Gegar Bagansa Sdn Bhd proposes a wider bandwidth of frequency band covered. The proposal put forward the block diagram of circuit changes as shown in **Figure Q3**. Gegar Bagansa Sdn Bhd claims the circuit being proposed could achieve the following:

- main purpose is to amplify the input voltage
- the closed-loop gain is at least 70% of the open-loop gain
- the open-loop gain, A , is not less than 1000.

- (a) Design a feedback circuit as shown in **Figure Q3** by determining the circuit configuration and its corresponding attenuation (feedback network) value. Assume $A\beta \gg 1$.

(6 marks)

- (b) Determine the following:

- (i) ratio $\frac{Z_{if}}{Z_i}$
- (ii) ratio $\frac{Z_{of}}{Z_o}$
- (iii) ratio $\frac{BW_f}{BW}$
- (iv) ratio $\frac{A_f}{A}$

(10 marks)

- (c) Analyse the drawback of implementing the circuit design shown in **Figure Q3** related to mobile communication service in targeted area.

(4 marks)

Q4 As a design engineer in IMAO Electronics, you are assigned to design an oscillator circuit that satisfies the following requirements:

- the output signal has 0° phase shift
- frequency of oscillation at 500 Hz

- (a) Propose a circuit design that meets the requirements by showing:
- values of all required components
 - a complete circuit configuration

(12 marks)

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- (b) Predict the possible output waveform and analyse its related application. Support your answer by showing input-output waveform and the corresponding gain. (8 marks)

Q5 (a) **Figure Q5(a)** is a full wave bridge circuit with a capacitor filter. Given capacitor, $C = 1000 \mu\text{F}$, DC current, $I_{dc} = 0.1 \text{ A}$ and forward diode voltage, $V_{diode} = 0.7 \text{ V}$.

- (i) Calculate the peak voltage at secondary winding, $V_{p(sec)}$, output average voltage, V_{dc} and peak-to-peak ripple voltage, $V_{r(p-p)}$

(6 marks)

- (ii) Draw the output waveforms of V_{sec} and V_o .

(4 marks)

- (b) An additional RC filter is connected to the circuit in **Figure Q5(a)**. Compare and conclude on the old and new ripple factor (%) if the value R and C are 50Ω and $100 \mu\text{F}$, respectively. Use $R_L = 100 \Omega$.

(6 marks)

- (c) Determine the minimum and maximum output voltages for voltage regulator in **Figure Q5(c)** if given $R_1 = 200 \Omega$, $R_2 = 5 \text{ k}\Omega$. Assume $I_{ADJ} = 50 \mu\text{A}$ and $V_{ref} = 1.5 \text{ V}$.

(4 marks)

- END OF QUESTIONS -

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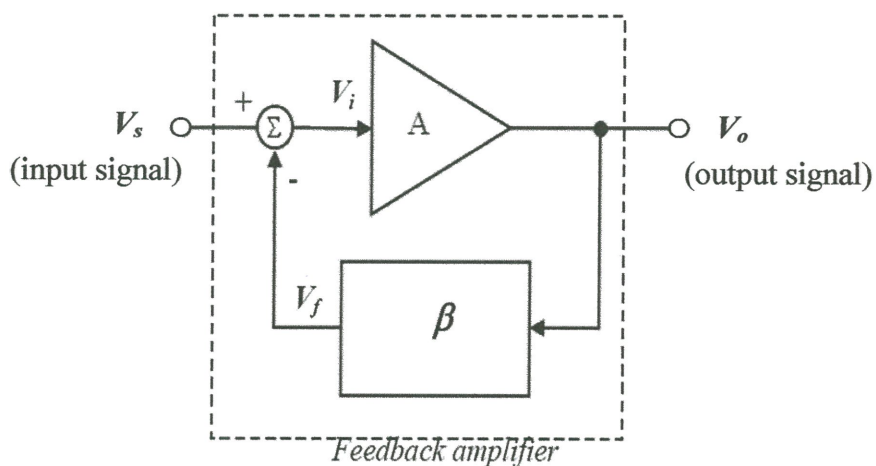


Figure Q3

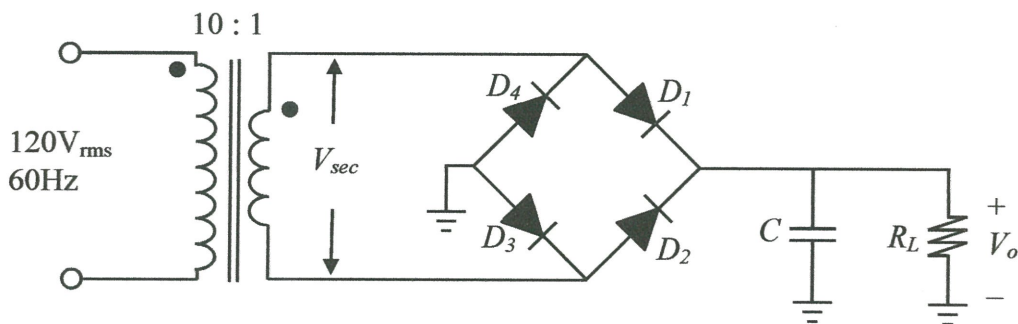
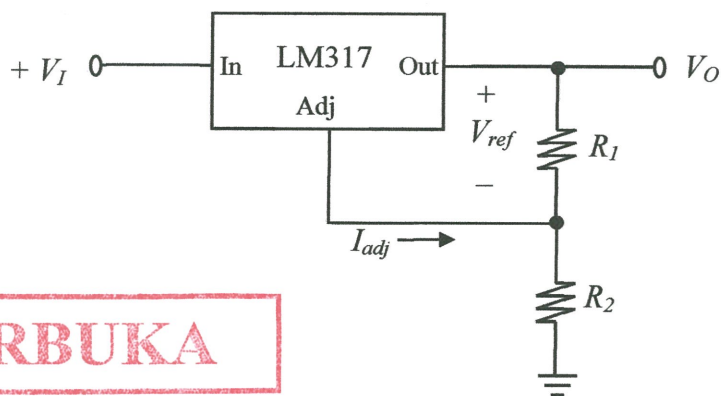


Figure Q5(a)



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Figure Q5(c)

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Table 1 List of formula

Inverting Amplifier	$A_v = \frac{V_o}{V_i} = -\frac{R_f}{R_1}$
Non-Inverting Amplifier	$A_v = \frac{V_o}{V_i} = 1 + \frac{R_f}{R_1}$
Inverting Summing Amplifier	$V_o = -\left(\frac{R_f}{R_1}V_1 + \frac{R_f}{R_2}V_2 + \frac{R_f}{R_3}V_3\right)$
Non-Inverting Summing Amplifier	$V_o = \left(1 + \frac{R_f}{R_1}\right)\left(\frac{R_B}{R_A + R_B}V_A + \frac{R_A}{R_A + R_B}V_B\right)$
Subtracting Amplifier	$V_o = \left(1 + \frac{R_f}{R_1}\right)\left(\frac{R_3}{R_2 + R_3}V_2 - \frac{R_f}{R_1 + R_f}V_1\right)$
Instrumentation Amplifier	$A_T = A_1 A_2 = \frac{v_o}{v_{in}} = \left(1 + \frac{2R}{R_x}\right)\left(\frac{R_4}{R_3}\right)$
Integrator	$V_o(t) = -\frac{1}{RC} \int_{t_0}^{t_1} V_i(t) dt + V_o(t_0)$
Differentiator	$V_o(t) = -RC \frac{dV_i(t)}{dt}$
Schmitt Trigger	$V_{UTP \text{ or } LTP} = \frac{R_2}{R_1 + R_2}(\pm V_{out(max)}) + \frac{R_1}{R_1 + R_2}(V_{REF})$
Cut-off frequency for a filter	$f_c = \frac{1}{2\pi RC}$
1 st order Low Pass Filter	$A_v(s) = \frac{V_o}{V_i} = \left(1 + \frac{R_F}{R_1}\right)\left(\frac{1}{1 + sRC}\right)$
2 nd order Low pass filter	$A_v(s) = \frac{V_o}{V_i}(s) = \frac{A_{VO}}{(RCs)^2 + (3 - A_{VO})RCs + 1}$
1 st order High Pass Filter	$A_v(s) = \frac{V_o}{V_i} = \left(1 + \frac{R_F}{R_1}\right)\left(\frac{1}{1 + \frac{1}{sRC}}\right)$



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Table 1 List of formula (Cont..)

2 nd order High Pass Filter	$A_v(s) = \frac{V_o(s)}{V_i(s)} = \frac{A_{vO}}{(sRC)^2 + \frac{3-A_{vO}}{sRC} + 1}$
Negative feedback – Gain	$A_f = \frac{V_o}{V_s} = \frac{A}{1 + \beta A}$
Positive feedback – Gain	$A_f = \frac{A}{1 - \beta A}$
Phase shift oscillator	$\beta = \frac{V_F}{V_o} = \frac{1}{\left(1 - \frac{5}{\omega^2 R^2 C^2}\right) + j\left(\frac{1}{\omega^3 R^3 C^3} - \frac{6}{\omega RC}\right)}$ $\text{or } \beta = \frac{V_F}{V_o} = \frac{1}{(1 - 5\omega^2 R^2 C^2) + j(6\omega RC - \omega^3 R^3 C^3)}$ $f_o = \frac{1}{2\pi RC\sqrt{6}} \quad \text{or } f_o = \frac{\sqrt{6}}{2\pi RC}$
Wien bridge oscillator	$f_o = \frac{1}{2\pi\sqrt{R_1 R_2 C_1 C_2}}$
Colpitts Oscillator	$f_o = \frac{1}{2\pi\sqrt{LC_{eq}}} \quad C_{eq} = \frac{C_1 C_2}{C_1 + C_2}$
Hartley Oscillator	$f_o = \frac{1}{2\pi\sqrt{CL_{eq}}} \quad L_{eq} = L_1 + L_2$
UJT relaxation oscillator	$f_o = \frac{1}{R_T C_T \ln[1/(1-\eta)]}$
Square-wave Oscillator	$f = \frac{1}{T} = \frac{1}{2RC \ln\left(\frac{1+\beta}{1-\beta}\right)} \quad \beta = \frac{R_3}{R_3 + R_2}$

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Table 1 List of formula (Cont..)

Triangular-wave Oscillator	$f = \frac{1}{4R_1C} \frac{R_2}{R_3}$
Capacitor voltage	$v_c(t) = v_c(0) + (v_c(\infty) - v_c(0)) \left(1 - e^{-t/\tau}\right)$ $= v_c(\infty) + (v_c(0) - v_c(\infty)) e^{-t/\tau}$
Astable Multivibrator	$T_m = t_1 = \tau_2 \ln 2 = 0.693(R_1 + R_2)C_1$ $T_s = t_2 = \tau_2 \ln 2 = 0.693R_2C_1$ $T = T_m + T_s$ $f = \frac{1.44}{(R_1 + 2R_2)C_1}$ $D = \frac{T_m}{T_m + T_s} \times 100\% = \frac{R_1 + R_2}{R_1 + 2R_2} \times 100\%$
Monostable Multivibrator	$T = 1.1 R_1 C_1$
Ripple Factor	$\% r = \frac{\text{ripple voltage (rms)}}{\text{dc voltage}} = \frac{V_{r(rms)}}{V_{dc}} \times 100$
Half-wave rectifier with a filter	$V_{r(rms)} = \frac{V_{r(p-p)}}{2\sqrt{3}} \approx \frac{V_{o(p)}}{2\sqrt{3} f C R_L}$ $V_{o(DC)} = V_{o(p)} - \frac{V_{r(p-p)}}{2} \qquad V_{r(p-p)} \approx \frac{V_{o(p)}}{f C R_L} = \frac{I_{o(DC)}}{f C}$ $r = \frac{V_{r(rms)}}{V_{DC}} \approx \frac{1}{2\sqrt{3} f C R_L}$
Full-wave rectifier with a filter	$V_{r(rms)} = \frac{V_{r(p-p)}}{2\sqrt{3}} \approx \frac{V_{o(p)}}{4\sqrt{3} f C R_L} = \frac{I_{DC}}{4\sqrt{3} f C}$ $V_{o(DC)} = V_{o(p)} - \frac{V_{r(p-p)}}{2}$ $V_{r(p-p)} = \frac{I_{o(DC)}}{2 f C} \approx \frac{V_{o(p)}}{2 f C R_L}$



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	$r = \frac{V_{r(rms)}}{V_{DC}} \approx \frac{1}{4\sqrt{3}fCR_L}$
Rectifier with Additional RC filter	$V'_{r(rms)} \approx \frac{X_C}{R} V_{r(rms)}$
Inductor Filter	$r = \frac{R_L}{3\sqrt{2}\omega L}$
Shunt regulator	$V_o \cong V_B \left(\frac{R_1 + R_2}{R_2} \right) \quad V_B = V_Z + V_{BE}$ $V_o \cong \left(\frac{R_1 + R_2}{R_2} \right) (V_Z)$
Series regulator	$V_o = \frac{R_1 + R_2}{R_1} (V_Z + V_{BE}) \quad V_o = V_Z \left(\frac{R_1 + R_2}{R_1} \right)$
Adjustable IC regulator	$V_o = V_{ref} \left(1 + \frac{R_2}{R_1} \right) + I_{adj} R_2$

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