



UNIVERSITI TUN HUSSEIN ONN MALAYSIA

**FINAL EXAMINATION
SEMESTER II
SESSION 2013/2014**

COURSE NAME : ELECTROMAGNETIC FIELDS AND WAVES
COURSE CODE : BEB 20303
PROGRAMME : BEJ
EXAMINATION DATE : JUNE 2014
DURATION : 3 HOURS
INSTRUCTION : **SECTION A – ANSWER ALL QUESTIONS**
SECTION B – ANSWER TWO (2)
QUESTIONS ONLY

THIS QUESTION PAPER CONSISTS OF **THIRTEEN (13)** PAGES

SECTION A – ANSWER ALL QUESTIONS

Q1 (a) List **ONE (1)** surrounding phenomenon on magnetostatic concept and discuss the working principles of the phenomenon based on the definition of Biot Savart's Law.

(5 marks)

(b) State **THREE (3)** similarities and difference between Electric Field and Magnetic Field

(6 marks)

(c) A rectangular conducting loop shown in **Figure Q1 (c)** lies in the $z = 0$ plane and carries a current I in the counterclockwise direction. Prove that at the center of the loop, the magnetic field intensity is given by $H = \frac{8.1 I}{4 \pi a} \hat{z}$.

(14 marks)

Q2 (a) Indicate whether electromotive force (EMF) induced in the loop of each of the following situations is clockwise, counterclockwise, or zero (EMF not induced). Justify your answer.

(i) Magnetic field through a wire loop is pointed upwards and increasing with time, as shown in **Figure Q2 (a)(i)**.

(ii) A rectangular wire loop is pulled away from a long wire carrying current I in the direction shown in **Figure Q2 (a)(ii)**.

(iii) A rectangular wire loop is pulled upward through a uniform magnetic field that point out of the screen penetrating the bottom half of the loop, as shown in **Figure Q2 (a)(iii)**.

- (iv) A rectangular wire loop is pulled sideways through a uniform magnetic field that points out of the screen penetrating the bottom half of the loop, as shown in **Figure Q2 (a)(iv)**. Justify your answers.

(10 marks)

- (b) A plane of wingspan of 30 m flies through a vertical magnetic field of strength, $B = 5 \times 10^{-4}$ T. Calculate the electromotive force (EMF) induced across the wing tips if the plane velocity is 150 m/s. Briefly explain why the horizontal component of the Earth's magnetic field does not contribute to the EMF between the wing tips of the plane.

(7 marks)

- (c) A square loop with length $l = 5$ cm on each side is placed in a uniform magnetic field, $B = 5 \times 10^{-6}$ T pointing into the page. During a time interval, $\Delta t = 2$ s, the loop is pulled from its two edges and turned into a rhombus with angle, $\theta = 60^\circ$, as shown in the **Figure Q2 (c)**. Assuming that the total resistance of the loop is $R = 10 \Omega$, calculate the average induced current in the loop I and its direction.

(8 marks)

SECTION B – ANSWER TWO (2) QUESTIONS ONLY

- Q3** (a) ‘An isolated magnetic charge does not exist’. Justify this statement. (5 marks)
- (b) Consider an infinitely long coaxial transmission line consisting of two concentric cylinders as shown in **Figure Q3(a)**.
- (i) By assuming the current distribution is uniformly distributed in both conductors, determine the magnetic field intensity, H along the Amperian path for all possible **SIX (6)** regions. (16 marks)
- (ii) Draw the magnetic flux lines which indicates the intensity of the magnetic field intensity, H . (4 marks)
- Q4** A spherical capacitor is formed by two metallic spheres of radius a (inner sphere) and b (outer sphere) with the separation between spheres d is as shown in **Figure Q4**. The charge on the inner sphere is $+Q$ and that on the outer sphere is $-Q$. The region in between the spheres is filled with dielectric material with dielectric constant of ϵ_r .
- (a) State the law that can be used to find the total electric flux in the region between the spheres. Explain the law in the form of a sentence. (3 marks)
- (b) Using the definition of law in **Q4 (a)**, deduce the general formulation for calculating the electric field intensity in the region between the spheres. (6 marks)

- (c) Calculate the capacitance of the system. (5 marks)
- (d) What is the capacitance of the isolated inner sphere? State clearly your assumption for the solution. (4 marks)
- (e) If the separation between the two spheres d is very small such that $d \ll a$, what is the capacitance of this system? State clearly your approximation for the solution. (4 marks)
- (f) From Q4 (b) – Q4 (e), how a capacitance value of a two conductors system can be controlled? (3 marks)

- Q5** (a) Consider a magnetic field intensity, $\vec{H} = 25 \sin(2 \times 10^8 t + 6x) \hat{a}_y$ mA/m. If the wave propagating through a nonmagnetic medium ($\mu = \mu_0$), determine:
- (i) The direction of wave propagation, k ,
 - (ii) The permittivity of the medium, ϵ ,
 - (iii) The electric field intensity, E_0 .
- (10 marks)
- (b) Given a 60-MHz plane wave travelling in the (-) x- direction in dry soil with relative permittivity, $\epsilon_r = 4$ has an electric field polarized along the (+) z- direction. By assuming the dry soil to be approximately lossless, and given that the magnetic field has a peak value of 10 (mA/m) and that its value was measured to be 7 (mA/m) at $t = 0$ and $x = -0.75$, develop a complete expressions for the wave's electric and magnetic fields. (15 marks)

- END OF QUESTIONS -

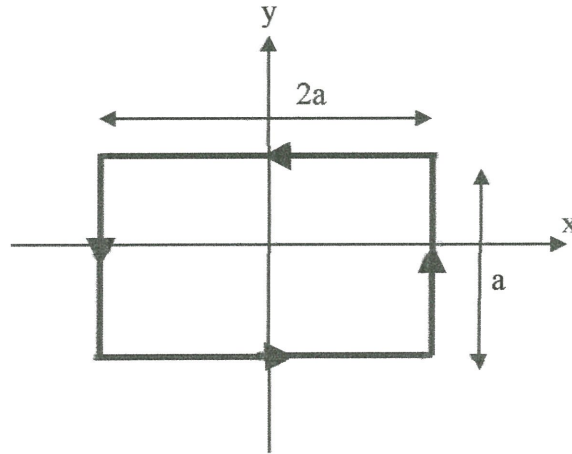
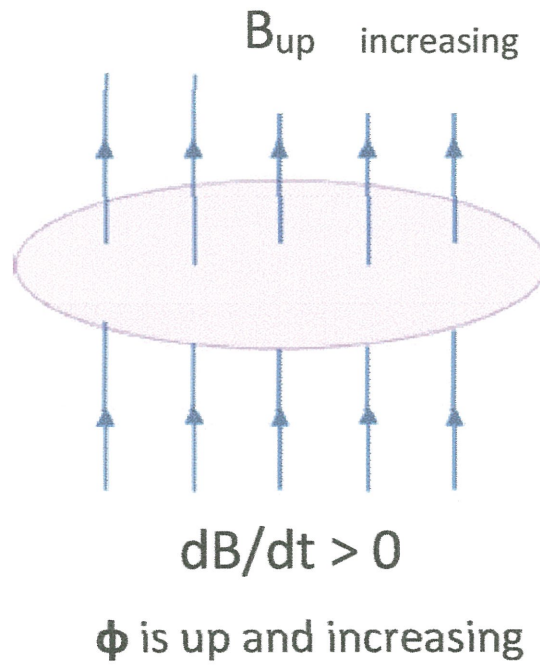
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**FIGURE Q1 (c)****FIGURE Q2 (a) (i)**

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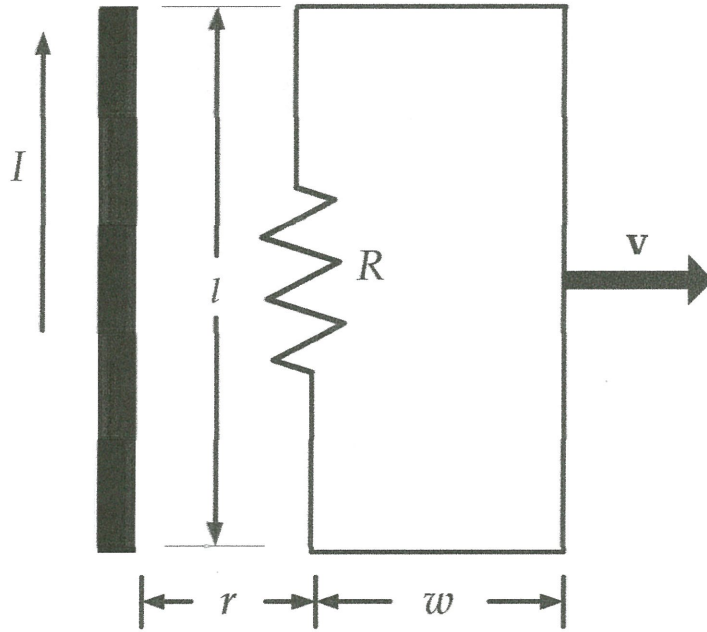


FIGURE Q2 (a) (ii)

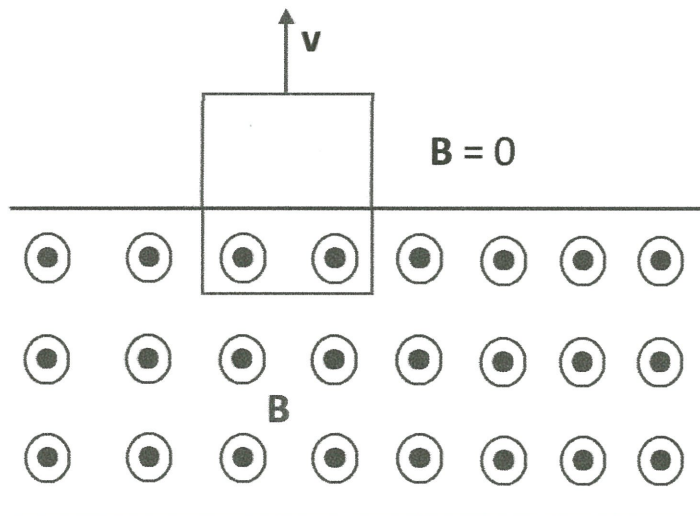


FIGURE Q2 (a) (iii)

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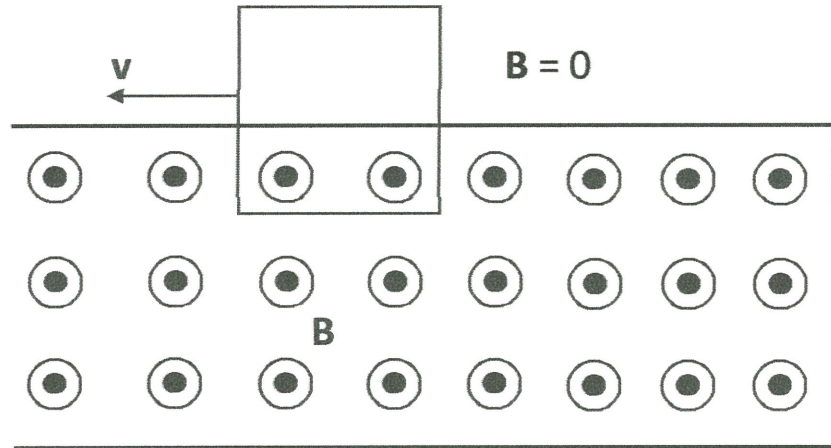


FIGURE Q2 (a) (iv)

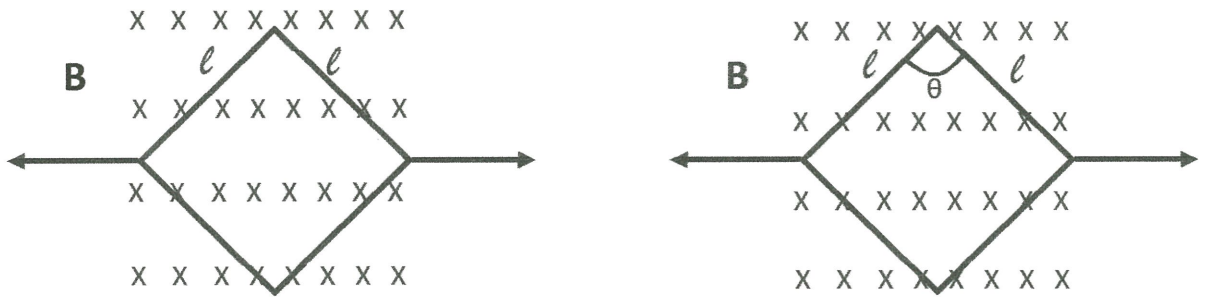


FIGURE Q2 (c)

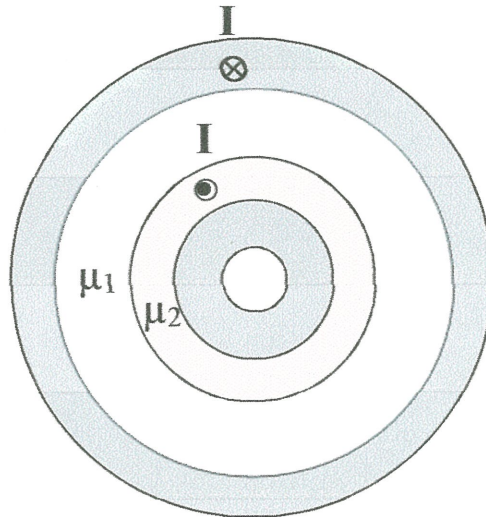
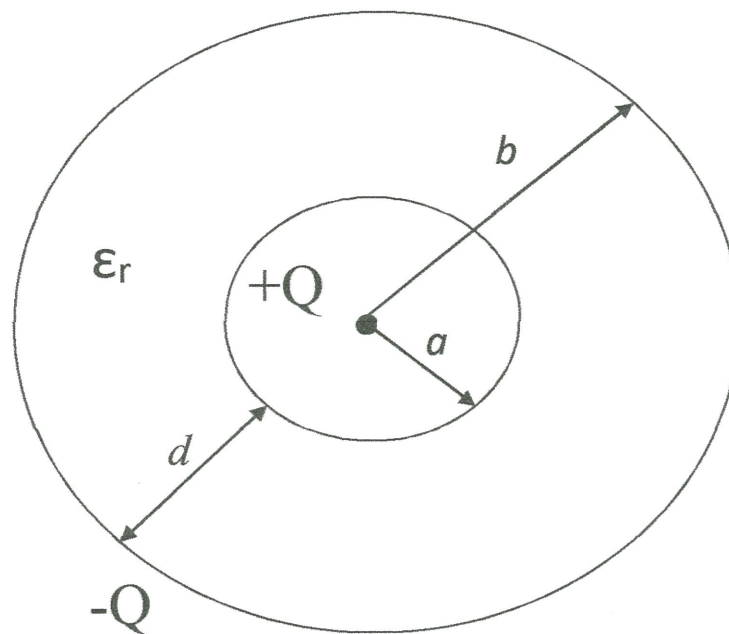
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**FIGURE Q3 (a)****FIGURE Q4**

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Formula

Gradient

$$\nabla f = \frac{\partial f}{\partial x} \hat{\mathbf{x}} + \frac{\partial f}{\partial y} \hat{\mathbf{y}} + \frac{\partial f}{\partial z} \hat{\mathbf{z}}$$

$$\nabla f = \frac{\partial f}{\partial r} \hat{\mathbf{r}} + \frac{1}{r} \frac{\partial f}{\partial \phi} \hat{\boldsymbol{\phi}} + \frac{\partial f}{\partial z} \hat{\mathbf{z}}$$

$$\nabla f = \frac{\partial f}{\partial R} \hat{\mathbf{R}} + \frac{1}{R} \frac{\partial f}{\partial \theta} \hat{\boldsymbol{\theta}} + \frac{1}{R \sin \theta} \frac{\partial f}{\partial \phi} \hat{\boldsymbol{\phi}}$$

Divergence

$$\nabla \cdot \vec{A} = \frac{\partial A_x}{\partial x} + \frac{\partial A_y}{\partial y} + \frac{\partial A_z}{\partial z}$$

$$\nabla \cdot \vec{A} = \frac{1}{r} \left[\frac{\partial(rA_r)}{\partial r} \right] + \frac{1}{r} \frac{\partial A_\phi}{\partial \phi} + \frac{\partial A_z}{\partial z}$$

$$\nabla \cdot \vec{A} = \frac{1}{R^2} \frac{\partial(R^2 A_R)}{\partial R} + \frac{1}{R \sin \theta} \left[\frac{\partial(A_\theta \sin \theta)}{\partial \theta} \right] + \frac{1}{R \sin \theta} \frac{\partial A_\phi}{\partial \phi}$$

Curl

$$\nabla \times \vec{A} = \left(\frac{\partial A_z}{\partial y} - \frac{\partial A_y}{\partial z} \right) \hat{\mathbf{x}} + \left(\frac{\partial A_x}{\partial z} - \frac{\partial A_z}{\partial x} \right) \hat{\mathbf{y}} + \left(\frac{\partial A_y}{\partial x} - \frac{\partial A_x}{\partial y} \right) \hat{\mathbf{z}}$$

$$\nabla \times \vec{A} = \left(\frac{1}{r} \frac{\partial A_z}{\partial \phi} - \frac{\partial A_\phi}{\partial z} \right) \hat{\mathbf{r}} + \left(\frac{\partial A_r}{\partial z} - \frac{\partial A_z}{\partial r} \right) \hat{\boldsymbol{\phi}} + \frac{1}{r} \left(\frac{\partial(rA_\phi)}{\partial r} - \frac{\partial A_r}{\partial \phi} \right) \hat{\mathbf{z}}$$

$$\nabla \times \vec{A} = \frac{1}{R \sin \theta} \left[\frac{\partial(\sin \theta A_\phi)}{\partial \theta} - \frac{\partial A_\theta}{\partial \phi} \right] \hat{\mathbf{R}} + \frac{1}{R} \left[\frac{1}{\sin \theta} \frac{\partial A_R}{\partial \phi} - \frac{\partial(RA_\phi)}{\partial R} \right] \hat{\boldsymbol{\theta}} + \frac{1}{R} \left[\frac{\partial(RA_\theta)}{\partial R} - \frac{\partial A_R}{\partial \theta} \right] \hat{\boldsymbol{\phi}}$$

Laplacian

$$\nabla^2 f = \frac{\partial^2 f}{\partial x^2} + \frac{\partial^2 f}{\partial y^2} + \frac{\partial^2 f}{\partial z^2}$$

$$\nabla^2 f = \frac{1}{r} \frac{\partial}{\partial r} \left(r \frac{\partial f}{\partial r} \right) + \frac{1}{r^2} \frac{\partial^2 f}{\partial \phi^2} + \frac{\partial^2 f}{\partial z^2}$$

$$\nabla^2 f = \frac{1}{R^2} \frac{\partial}{\partial R} \left(R^2 \frac{\partial f}{\partial R} \right) + \frac{1}{R^2 \sin \theta} \frac{\partial}{\partial \theta} \left(\sin \theta \frac{\partial f}{\partial \theta} \right) + \frac{1}{R^2 \sin^2 \theta} \left(\frac{\partial^2 f}{\partial \phi^2} \right)$$

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	Cartesian	Cylindrical	Spherical
Coordinate parameters	x, y, z	r, ϕ, z	R, θ, ϕ
Vector \vec{A}	$A_x \hat{x} + A_y \hat{y} + A_z \hat{z}$	$A_r \hat{r} + A_\phi \hat{\phi} + A_z \hat{z}$	$A_R \hat{R} + A_\theta \hat{\theta} + A_\phi \hat{\phi}$
Magnitude \vec{A}	$\sqrt{A_x^2 + A_y^2 + A_z^2}$	$\sqrt{A_r^2 + A_\phi^2 + A_z^2}$	$\sqrt{A_R^2 + A_\theta^2 + A_\phi^2}$
Position vector, \vec{OP}	$x_1 \hat{x} + y_1 \hat{y} + z_1 \hat{z}$ for point $P(x_1, y_1, z_1)$	$r_1 \hat{r} + z_1 \hat{z}$ for point $P(r_1, \phi_1, z_1)$	$R_1 \hat{R}$ for point $P(R_1, \theta_1, \phi_1)$
Unit vector product	$\hat{x} \cdot \hat{x} = \hat{y} \cdot \hat{y} = \hat{z} \cdot \hat{z} = 1$ $\hat{x} \cdot \hat{y} = \hat{y} \cdot \hat{z} = \hat{z} \cdot \hat{x} = 0$ $\hat{x} \times \hat{y} = \hat{z}$ $\hat{y} \times \hat{z} = \hat{x}$ $\hat{z} \times \hat{x} = \hat{y}$	$\hat{r} \cdot \hat{r} = \hat{\phi} \cdot \hat{\phi} = \hat{z} \cdot \hat{z} = 1$ $\hat{r} \cdot \hat{\phi} = \hat{\phi} \cdot \hat{z} = \hat{z} \cdot \hat{r} = 0$ $\hat{r} \times \hat{\phi} = \hat{z}$ $\hat{\phi} \times \hat{z} = \hat{r}$ $\hat{z} \times \hat{r} = \hat{\phi}$	$\hat{R} \cdot \hat{R} = \hat{\theta} \cdot \hat{\theta} = \hat{\phi} \cdot \hat{\phi} = 1$ $\hat{R} \cdot \hat{\theta} = \hat{\theta} \cdot \hat{\phi} = \hat{\phi} \cdot \hat{R} = 0$ $\hat{R} \times \hat{\theta} = \hat{\phi}$ $\hat{\theta} \times \hat{\phi} = \hat{R}$ $\hat{\phi} \times \hat{R} = \hat{\theta}$
Dot product $\vec{A} \cdot \vec{B}$	$A_x B_x + A_y B_y + A_z B_z$	$A_r B_r + A_\phi B_\phi + A_z B_z$	$A_R B_R + A_\theta B_\theta + A_\phi B_\phi$
Cross product $\vec{A} \times \vec{B}$	$\begin{vmatrix} \hat{x} & \hat{y} & \hat{z} \\ A_x & A_y & A_z \\ B_x & B_y & B_z \end{vmatrix}$	$\begin{vmatrix} \hat{r} & \hat{\phi} & \hat{z} \\ A_r & A_\phi & A_z \\ B_r & B_\phi & B_z \end{vmatrix}$	$\begin{vmatrix} \hat{R} & \hat{\theta} & \hat{\phi} \\ A_R & A_\theta & A_\phi \\ B_R & B_\theta & B_\phi \end{vmatrix}$
Differential length, $d\vec{\ell}$	$dx \hat{x} + dy \hat{y} + dz \hat{z}$	$dr \hat{r} + r d\phi \hat{\phi} + dz \hat{z}$	$dR \hat{R} + R d\theta \hat{\theta} + R \sin \theta d\phi \hat{\phi}$
Differential surface, $d\vec{s}$	$\vec{ds}_x = dy dz \hat{x}$ $\vec{ds}_y = dx dz \hat{y}$ $\vec{ds}_z = dx dy \hat{z}$	$\vec{ds}_r = rd\phi dz \hat{r}$ $\vec{ds}_\phi = dr dz \hat{\phi}$ $\vec{ds}_z = r dr d\phi \hat{z}$	$\vec{ds}_R = R^2 \sin \theta d\theta d\phi \hat{R}$ $\vec{ds}_\theta = R \sin \theta dR d\phi \hat{\theta}$ $\vec{ds}_\phi = R dR d\theta \hat{\phi}$
Differential volume, $d\vec{v}$	$dx dy dz$	$r dr d\phi dz$	$R^2 \sin \theta dR d\theta d\phi$

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Transformation	Coordinate Variables	Unit Vectors	Vector Components
Cartesian to Cylindrical	$r = \sqrt{x^2 + y^2}$ $\phi = \tan^{-1}(y/x)$ $z = z$	$\hat{\mathbf{r}} = \hat{\mathbf{x}} \cos \phi + \hat{\mathbf{y}} \sin \phi$ $\hat{\boldsymbol{\phi}} = -\hat{\mathbf{x}} \sin \phi + \hat{\mathbf{y}} \cos \phi$ $\hat{\mathbf{z}} = \hat{\mathbf{z}}$	$A_r = A_x \cos \phi + A_y \sin \phi$ $A_\phi = -A_x \sin \phi + A_y \cos \phi$ $A_z = A_z$
Cylindrical to Cartesian	$x = r \cos \phi$ $y = r \sin \phi$ $z = z$	$\hat{\mathbf{x}} = \hat{\mathbf{r}} \cos \phi - \hat{\boldsymbol{\phi}} \sin \phi$ $\hat{\mathbf{y}} = \hat{\mathbf{r}} \sin \phi + \hat{\boldsymbol{\phi}} \cos \phi$ $\hat{\mathbf{z}} = \hat{\mathbf{z}}$	$A_x = A_r \cos \phi - A_\phi \sin \phi$ $A_y = A_r \sin \phi + A_\phi \cos \phi$ $A_z = A_z$
Cartesian to Spherical	$R = \sqrt{x^2 + y^2 + z^2}$ $\theta = \tan^{-1}(\sqrt{x^2 + y^2}/z)$ $\phi = \tan^{-1}(y/x)$	$\hat{\mathbf{R}} = \hat{\mathbf{x}} \sin \theta \cos \phi$ $\quad + \hat{\mathbf{y}} \sin \theta \sin \phi + \hat{\mathbf{z}} \cos \theta$ $\hat{\boldsymbol{\theta}} = \hat{\mathbf{x}} \cos \theta \cos \phi$ $\quad + \hat{\mathbf{y}} \cos \theta \sin \phi - \hat{\mathbf{z}} \sin \theta$ $\hat{\boldsymbol{\phi}} = -\hat{\mathbf{x}} \sin \phi + \hat{\mathbf{y}} \cos \phi$	$A_R = A_x \sin \theta \cos \phi$ $\quad + A_y \sin \theta \sin \phi + A_z \cos \theta$ $A_\theta = A_x \cos \theta \cos \phi$ $\quad + A_y \cos \theta \sin \phi - A_z \sin \theta$ $A_\phi = -A_x \sin \phi + A_y \cos \phi$
Spherical to Cartesian	$x = R \sin \theta \cos \phi$ $y = R \sin \theta \sin \phi$ $z = R \cos \theta$	$\hat{\mathbf{x}} = \hat{\mathbf{R}} \sin \theta \cos \phi +$ $\hat{\boldsymbol{\theta}} \cos \theta \cos \phi - \hat{\boldsymbol{\phi}} \sin \phi$ $\hat{\mathbf{y}} = \hat{\mathbf{R}} \sin \theta \sin \phi +$ $\hat{\boldsymbol{\theta}} \cos \theta \sin \phi + \hat{\boldsymbol{\phi}} \cos \phi$ $\hat{\mathbf{z}} = \hat{\mathbf{R}} \cos \theta - \hat{\boldsymbol{\theta}} \sin \theta$	$A_x = A_R \sin \theta \cos \phi$ $\quad + A_\theta \cos \theta \cos \phi - A_\phi \sin \phi$ $A_y = A_R \sin \theta \sin \phi$ $\quad + A_\theta \cos \theta \sin \phi + A_\phi \cos \phi$ $A_z = A_R \cos \theta - A_\theta \sin \theta$
Cylindrical to Spherical	$R = \sqrt{r^2 + z^2}$ $\theta = \tan^{-1}(r/z)$ $\phi = \phi$	$\hat{\mathbf{R}} = \hat{\mathbf{r}} \sin \theta + \hat{\mathbf{z}} \cos \theta$ $\hat{\boldsymbol{\theta}} = \hat{\mathbf{r}} \cos \theta - \hat{\mathbf{z}} \sin \theta$ $\hat{\boldsymbol{\phi}} = \hat{\boldsymbol{\phi}}$	$A_R = A_r \sin \theta + A_z \cos \theta$ $A_\theta = A_r \cos \theta - A_z \sin \theta$ $A_\phi = A_\phi$
Spherical to Cylindrical	$r = R \sin \theta$ $\phi = \phi$ $z = R \cos \theta$	$\hat{\mathbf{r}} = \hat{\mathbf{R}} \sin \theta + \hat{\boldsymbol{\theta}} \cos \theta$ $\hat{\boldsymbol{\phi}} = \hat{\boldsymbol{\phi}}$ $\hat{\mathbf{z}} = \hat{\mathbf{R}} \cos \theta - \hat{\boldsymbol{\theta}} \sin \theta$	$A_r = A_R \sin \theta + A_\theta \cos \theta$ $A_\phi = A_\phi$ $A_z = A_R \cos \theta - A_\theta \sin \theta$

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$Q = \int \rho_t dl,$ $Q = \int \rho_s dS,$ $Q = \int \rho_v dv$ $\bar{F}_{12} = \frac{Q_1 Q_2}{4\pi\epsilon_0 R^2} \hat{a}_{R_{12}}$ $\bar{E} = \frac{\bar{F}}{Q},$ $\bar{E} = \frac{Q}{4\pi\epsilon_0 R^2} \hat{a}_R$ $\bar{E} = \int \frac{\rho_t dl}{4\pi\epsilon_0 R^2} \hat{a}_R$ $\bar{E} = \int \frac{\rho_s dS}{4\pi\epsilon_0 R^2} \hat{a}_R$ $\bar{E} = \int \frac{\rho_v dv}{4\pi\epsilon_0 R^2} \hat{a}_R$ $\bar{D} = \epsilon \bar{E}$ $\psi_e = \int \bar{D} \cdot d\bar{S}$ $Q_{enc} = \oint_S \bar{D} \cdot d\bar{S}$ $\rho_v = \nabla \cdot \bar{D}$ $V_{AB} = - \int_A^B \bar{E} \cdot d\bar{l} = \frac{W}{Q}$ $V = \frac{Q}{4\pi\epsilon r}$ $V = \int \frac{\rho_t dl}{4\pi\epsilon r}$ $\oint \bar{E} \cdot d\bar{l} = 0$ $\nabla \times \bar{E} = 0$ $\bar{E} = -\nabla V$ $\nabla^2 V = 0$ $R = \frac{\ell}{\sigma S}$ $I = \int \bar{J} \cdot dS$	$d\bar{H} = \frac{Id\bar{l} \times \bar{R}}{4\pi R^3}$ $Id\bar{l} \equiv \bar{J}_s dS \equiv \bar{J} dv$ $\oint \bar{H} \cdot d\bar{l} = I_{enc} = \int \bar{J}_s dS$ $\nabla \times \bar{H} = \bar{J}$ $\psi_m = \int_s \bar{B} \cdot d\bar{S}$ $\psi_m = \oint \bar{B} \cdot d\bar{S} = 0$ $\psi_m = \oint \bar{A} \cdot d\bar{l}$ $\nabla \cdot \bar{B} = 0$ $\bar{B} = \mu \bar{H}$ $\bar{B} = \nabla \times \bar{A}$ $\bar{A} = \int \frac{\mu_0 Id\bar{l}}{4\pi R}$ $\nabla^2 \bar{A} = -\mu_0 \bar{J}$ $\bar{F} = Q(\bar{E} + \bar{u} \times \bar{B}) = m \frac{d\bar{u}}{dt}$ $d\bar{F} = Id\bar{l} \times \bar{B}$ $\bar{T} = \bar{r} \times \bar{F} = \bar{m} \times \bar{B}$ $\bar{m} = IS\hat{a}_n$ $V_{emf} = - \frac{\partial \psi}{\partial t}$ $V_{emf} = - \int \frac{\partial \bar{B}}{\partial t} \cdot d\bar{S}$ $V_{emf} = \int (\bar{u} \times \bar{B}) \cdot d\bar{l}$ $I_d = \int J_d \cdot d\bar{S}, J_d = \frac{\partial \bar{D}}{\partial t}$ $\gamma = \alpha + j\beta$ $\alpha = \omega \sqrt{\frac{\mu\epsilon}{2} \left[\sqrt{1 + \left[\frac{\sigma}{\omega\epsilon} \right]^2} - 1 \right]}$ $\beta = \omega \sqrt{\frac{\mu\epsilon}{2} \left[\sqrt{1 + \left[\frac{\sigma}{\omega\epsilon} \right]^2} + 1 \right]}$	$\bar{F}_1 = \frac{\mu I_1 I_2}{4\pi} \oint_{L1L2} \oint_{L1L2} \frac{d\bar{l}_1 \times (d\bar{l}_2 \times \hat{a}_{R_{21}})}{R_{21}^2}$ $ \eta = \frac{\sqrt{\mu/\epsilon}}{\left[1 + \left(\frac{\sigma}{\omega\epsilon} \right)^2 \right]^{1/4}}$ $\tan 2\theta_\eta = \frac{\sigma}{\omega\epsilon}$ $\tan \theta = \frac{\sigma}{\omega\epsilon} = \frac{\bar{J}_s}{\bar{J}_{ds}}$ $\delta = \frac{1}{\alpha}$ $\epsilon_0 = 8.854 \times 10^{-12} \text{ Fm}^{-1}$ $\mu_0 = 4\pi \times 10^{-7} \text{ Hm}^{-1}$ $\int \frac{dx}{(x^2 + c^2)^{3/2}} = \frac{x}{c^2(x^2 + c^2)^{1/2}}$ $\int \frac{xdx}{(x^2 + c^2)^{3/2}} = \frac{-1}{(x^2 + c^2)^{1/2}}$ $\int \frac{dx}{(x^2 \pm c^2)^{1/2}} = \ln(x + \sqrt{x^2 \pm c^2})$ $\int \frac{dx}{(x^2 + c^2)} = \frac{1}{c} \tan^{-1} \left(\frac{x}{c} \right)$ $\int \frac{xdx}{(x^2 + c^2)} = \frac{1}{2} \ln(x^2 + c^2)$ $\int \frac{xdx}{(x^2 + c^2)^{1/2}} = \sqrt{x^2 + c^2}$
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