



UTHM

Universiti Tun Hussein Onn Malaysia

UNIVERSITI TUN HUSSEIN ONN MALAYSIA

FINAL EXAMINATION SEMESTER II SESSION 2016/2017

COURSE NAME : ADVANCED STRUCTURAL ANALYSIS

COURSE CODE : BFS40103

PROGRAMME CODE : BFF

EXAMINATION DATE : JUNE 2017

DURATION : 3 HOURS

INSTRUCTION : ANSWER **FOUR (4)** QUESTIONS ONLY

THIS QUESTION PAPER CONSISTS OF **TEN (10)** PAGES

Q1 (a) List **THREE (3)** advantages and **THREE (3)** disadvantages of statically indeterminate structure.

(6 marks)

(b) A continuous indeterminate beam shown in **FIGURE Q1** is supported by rollers at point A and B, and pinned at point C. A 100 kN load is applied at 4 m from support A. Given $E = 200 \text{ GPa}$ and $I = 500 \times 10^6 \text{ mm}^4$. If support B is displaced 40 mm;

(i) Determine the compatibility equation

(2 marks)

(ii) Determine all reactions at supports

(13 marks)

(iii) Draw the shear force and bending moment diagram

(4 marks)

Q2 For the truss structure given in **FIGURE Q2**, use the stiffness method to determine;

(a) The local matrix for member 1 and 2.

(17 marks)

(b) The global matrix for the truss if local matrix for member 3 is given as;

$$[k_3] = AE \begin{bmatrix} 0.128 & 0.096 & -0.128 & -0.096 \\ 0.096 & 0.072 & -0.096 & -0.072 \\ -0.128 & -0.096 & 0.128 & 0.096 \\ -0.096 & -0.072 & 0.096 & 0.072 \end{bmatrix}$$

(8 marks)

Q3 The cross section of the structure is as shown in **FIGURE Q3**. The deck is supported by a row of steel pipe columns. The base of the columns are set in concrete pad footings

Q3 The cross section of the structure is as shown in **FIGURE Q3**. The deck is supported by a row of steel pipe columns. The base of the columns are set in concrete pad footings (restrained in X, Y and Z directions) while the top of the columns are supported laterally by the deck platform. The parameters are given as follows:

- i) Height of column, $H = 3.5$ m
- ii) Column is of tubular cross section shape with $D = 100$ mm and $d = 105$ mm
- iii) Modulus of Elasticity = 70 GPa ; Ultimate Stress $\sigma_{ultimate} = 260$ MPa
- iv) Design compressive load of each column $P_{applied} = 80$ kN
- v) Factor of Safety, $n = 3$

With respect to Euler's column buckling :-

- (a) Model the column support condition.

(3 marks)

- (b) Conduct calculation checks on the actual load carrying capacity of the column and compare with $P_{applied}$. State your findings.

(10 marks)

- (c) Provide solution of Q3(b) by showing relevant calculations and state your recommendation.

(12 marks)

- Q4** (a) Discuss **TWO (2)** reasons why yield line theory is safe under reinforced concrete slab although it is based on upper bond limit.

(4 marks)

- (b) Sketch the yield line pattern for the slabs shown in **FIGURE Q4(b)**.

(4 marks)

- (d) **FIGURE Q4(c)** shows an isotropic triangular slab subjected to a concentrated load, P of 50 kN and uniformly distributed load of 10 kN/m². Based on the yield line pattern shown in the figure, determine the ultimate resistance moment.

(17 marks)

- Q5** (a) State the assumptions that an engineer need to consider in plastic bending.
(3 marks)
- (b) Identify and sketch the possible collapse mechanisms for the structures shown in Figure **Q5(b)**.
(7 marks)
- (c) **FIGURE Q5(c)** shows a portal frame which carries point load P at point B and C respectively. Determine the value of the collapse load, P of the frame.
(15 marks)

– END OF QUESTIONS –

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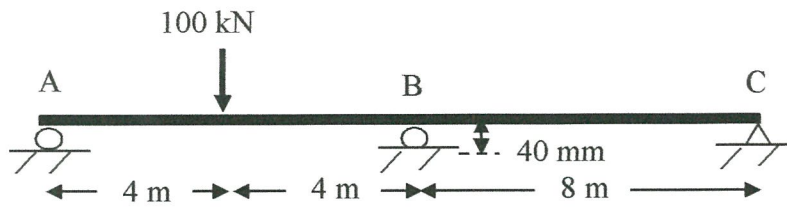


FIGURE Q1

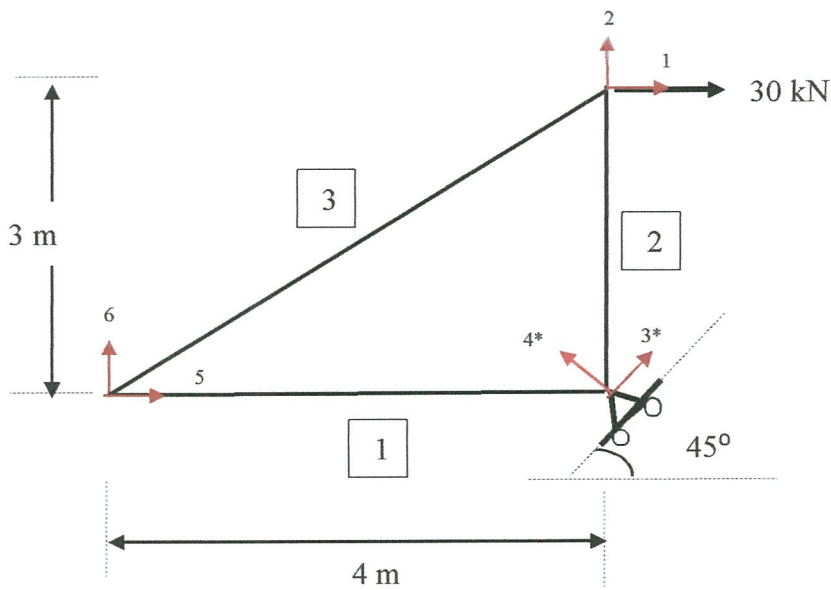


FIGURE Q2

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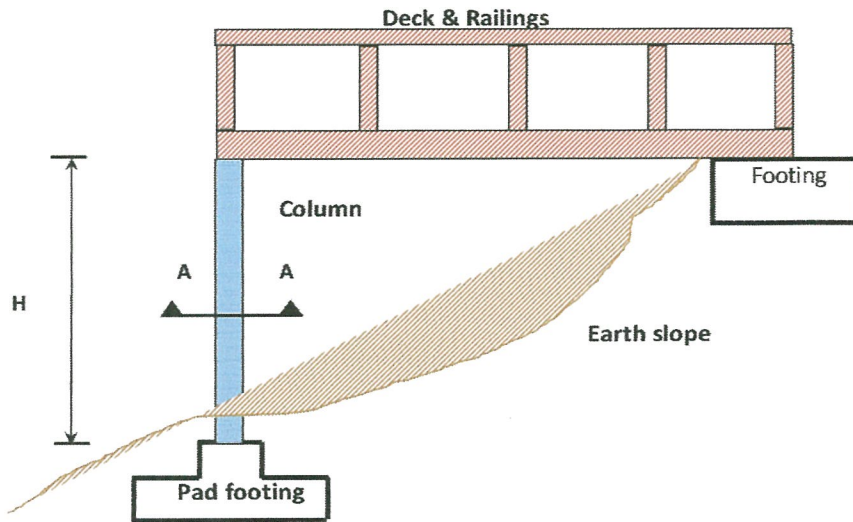
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SECTION A - A

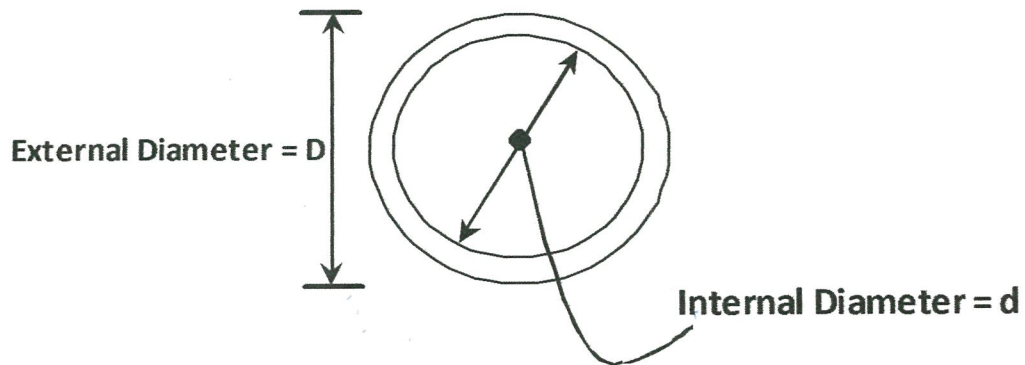


FIGURE Q3

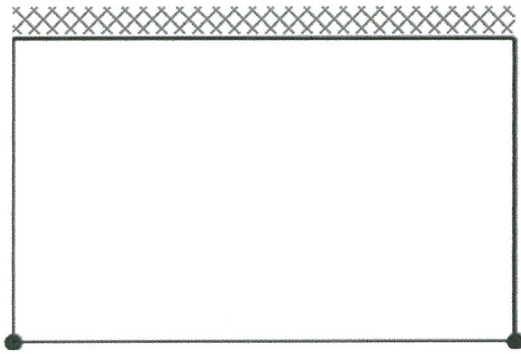
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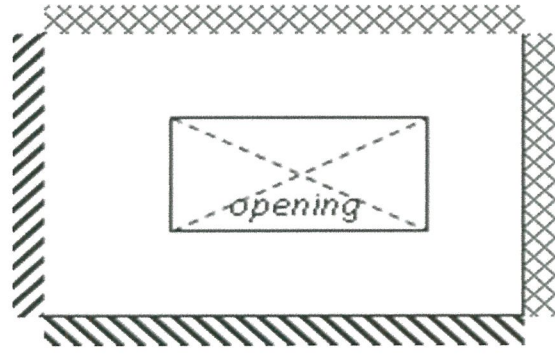
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(i)



(ii)

FIGURE Q4(b)

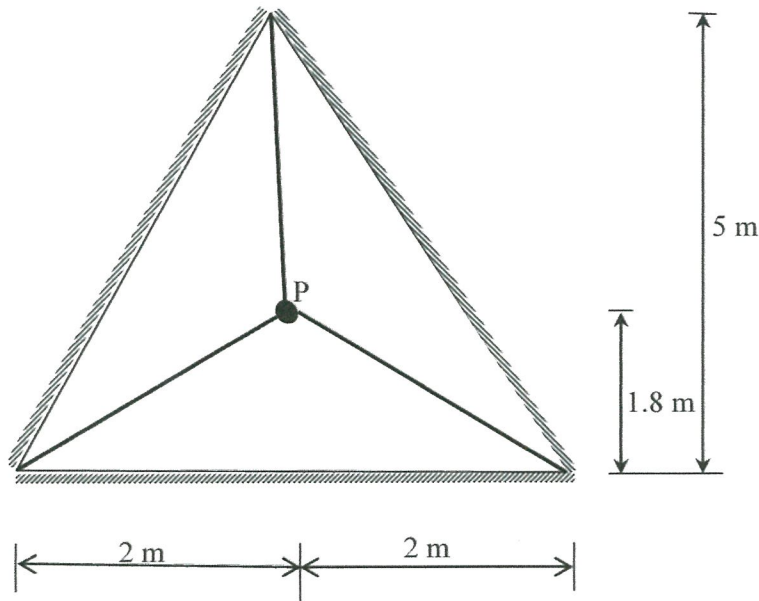


FIGURE Q4(c)

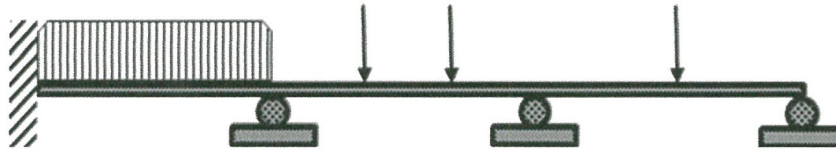
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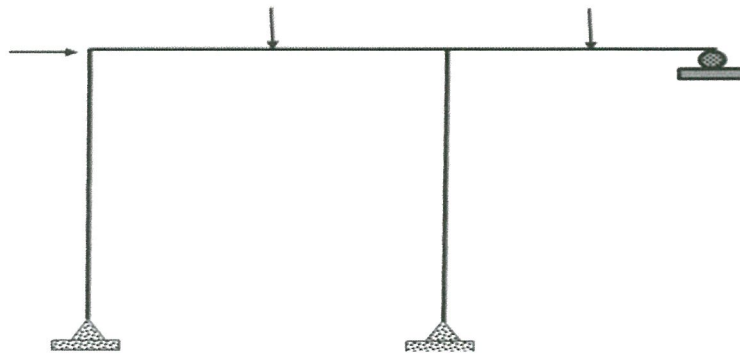
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(i)



(ii)

FIGURE Q5(b)

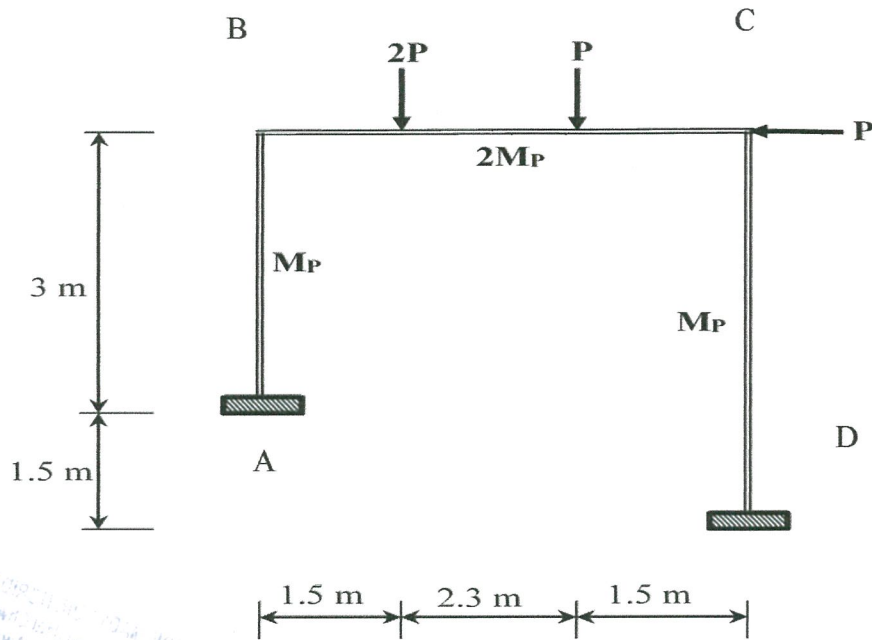


FIGURE Q5(c)

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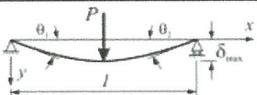
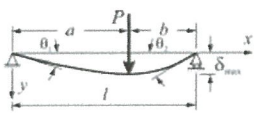
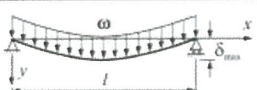

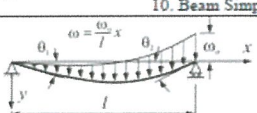
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The following information may be useful. The symbols have their usual meaning.

Beam Deflection Equation

BEAM DEFLECTION FORMULAS			
BEAM TYPE	SLOPE AT ENDS	DEFLECTION AT ANY SECTION IN TERMS OF x	MAXIMUM AND CENTER DEFLECTION
<p>6. Beam Simply Supported at Ends - Concentrated load P at the center</p> 	$\theta_1 = \theta_2 = \frac{Pl^2}{16EI}$	$y = \frac{Px}{12EI} \left(\frac{3l^2}{4} - x^2 \right)$ for $0 < x < \frac{l}{2}$	$\delta_{max} = \frac{Pl^3}{48EI}$
<p>7. Beam Simply Supported at Ends - Concentrated load P at any point</p> 	$\theta_1 = \frac{Pb(l^2 - b^2)}{6EI}$ $\theta_2 = \frac{Pab(2l - b)}{6EI}$	$y = \frac{Pbx}{6EI} (l^2 - x^2 - b^2)$ for $0 < x < a$ $y = \frac{Pb}{6EI} \left[\frac{l}{b}(x-a)^3 + (l^2 - b^2)x - x^3 \right]$ for $a < x < l$	$\delta_{max} = \frac{Pb(l^2 - b^2)^{3/2}}{9\sqrt{3}EI}$ at $x = \sqrt{(l^2 - b^2)}/\sqrt{3}$ $\delta = \frac{Pb}{48EI} (3l^2 - 4b^2)$ at the center, if $a > b$
<p>8. Beam Simply Supported at Ends - Uniformly distributed load ω (N/m)</p> 	$\theta_1 = \theta_2 = \frac{\omega l^3}{24EI}$	$y = \frac{\omega x}{24EI} (l^3 - 2lx^2 + x^3)$	$\delta_{max} = \frac{5\omega l^4}{384EI}$
<p>9. Beam Simply Supported at Ends - Couple moment M at the right end</p> 	$\theta_1 = \frac{Ml}{6EI}$ $\theta_2 = \frac{Ml}{3EI}$	$y = \frac{Mlx}{6EI} \left(1 - \frac{x^2}{l^2} \right)$	$\delta_{max} = \frac{Ml^2}{9\sqrt{3}EI}$ at $x = \frac{l}{\sqrt{3}}$ $\delta = \frac{Ml^2}{16EI}$ at the center
<p>10. Beam Simply Supported at Ends - Uniformly varying load: Maximum intensity ω_0 (N/m)</p> 	$\theta_1 = \frac{7\omega_0 l^3}{360EI}$ $\theta_2 = \frac{\omega_0 l^3}{45EI}$	$y = \frac{\omega_0 x}{360EI} (7l^4 - 10l^2 x^2 + 3x^4)$	$\delta_{max} = 0.00652 \frac{\omega_0 l^4}{EI}$ at $x = 0.519l$ $\delta = 0.00651 \frac{\omega_0 l^4}{EI}$ at the center

Member Stiffness Matrix for Truss

$$\mathbf{k} = \frac{AE}{L} \begin{bmatrix} N_x & N_y & F_x & F_y \\ \lambda_x^2 & \lambda_x \lambda_y & -\lambda_x^2 & -\lambda_x \lambda_y \\ \lambda_x \lambda_y & \lambda_y^2 & -\lambda_x \lambda_y & -\lambda_y^2 \\ -\lambda_x^2 & -\lambda_x \lambda_y & \lambda_x^2 & \lambda_x \lambda_y \\ -\lambda_x \lambda_y & -\lambda_y^2 & \lambda_x \lambda_y & \lambda_y^2 \end{bmatrix} \begin{bmatrix} N_x \\ N_y \\ F_x \\ F_y \end{bmatrix}$$

Where $\rightarrow \lambda_x = \frac{x_F - x_N}{L}$; $\lambda_y = \frac{y_F - y_N}{L}$

$$[\mathbf{k}^*] = [\mathbf{T}^T] \frac{AE}{L} \begin{bmatrix} 1 & -1 \\ -1 & 1 \end{bmatrix} [\mathbf{T}]$$

