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Universiti Tun Hussein Onn Malaysia

UNIVERSITI TUN HUSSEIN ONN MALAYSIA

**FINAL EXAMINATION
SEMESTER II
SESSION 2015/2016**

COURSE NAME : REINFORCED CONCRETE DESIGN 1

COURSE CODE : BFC 32102

PROGRAMME CODE : BFF

EXAMINATION DATE : JUNE / JULY 2016

DURATION : 2 HOURS

INSTRUCTION : 1. ANSWER ALL QUESTIONS FROM SECTION A AND THREE (3) QUESTIONS FROM SECTION B.

2. DESIGN SHOULD BE BASED ON:

BS EN 1990:2002+A1:2005

BS EN 1991-1-1:2002

BS EN 1992-1-1:2004

THIS PAPER CONSISTS OF SIXTEEN (16) PAGES

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SECTION A: ANSWER ALL QUESTIONS

- Q1** (a) Design situations of limit state can be divided into several categories. Name and briefly explain the design situations that are involved in the design of reinforced concrete structures.
(8 marks)
- (b) An architecture plan of second floor of residential house is shown in **FIGURE Q1**. By using an appropriate approach, produce a complete engineering layout of the floor plan.
(10 marks)
- (c) Based on the engineering layout in **Q1(b)**, draw the cross section X-X and propose the suitable size of the beams and slabs.
(7 marks)

SECTION B: ANSWER THREE (3) QUESTIONS ONLY

- Q2** A plan view of a terrace house is shown in **FIGURE Q2**. End beam 5/A-B is initially designed by considering rectangular shape with size 250 mm x 650 mm and singly reinforcement of 2H20. Other specifications of the design are given as follows:

| | |
|-------------------------------------|-------------------------|
| Characteristic strength of concrete | = C25/30 |
| Characteristic strength of steel | = 500 N/mm ² |
| Unit weight of concrete | = 25 kN/m ³ |
| Nominal cover | = 30 mm |
| Thickness of slab | = 125 mm |

- (a) Determine the moment resistance of section for end beam 5/A-B.
(6 marks)
- (b) If the actual variable and permanent actions are 3.0 kN/m² and 1.5 kN/m² (excluding selfweight) respectively, classify the type of flexural failure that may happen on the beam.
(12 marks)
- (c) Evaluate the required reinforcement area and compare the serviceability condition with the initial design.
(7 marks)

- Q5** **FIGURE Q5** shows the layout plan for the part of the third floor of library building. The concrete for slabs and beams are poured together and the thickness of the slab is 150 mm. The permanent and variable actions for slab are as follows:

| | | |
|---|---|------------------------|
| Ceiling and tile finishes | = | 1.75 kN/m ² |
| Variable action | = | 3.0 kN/m ² |
| Characteristic strength of concrete, f_{ck} | = | 25 N/mm ² |
| Characteristic strength of steel, f_{yk} | = | 500 N/mm ² |
| Concrete cover | = | 25 mm |

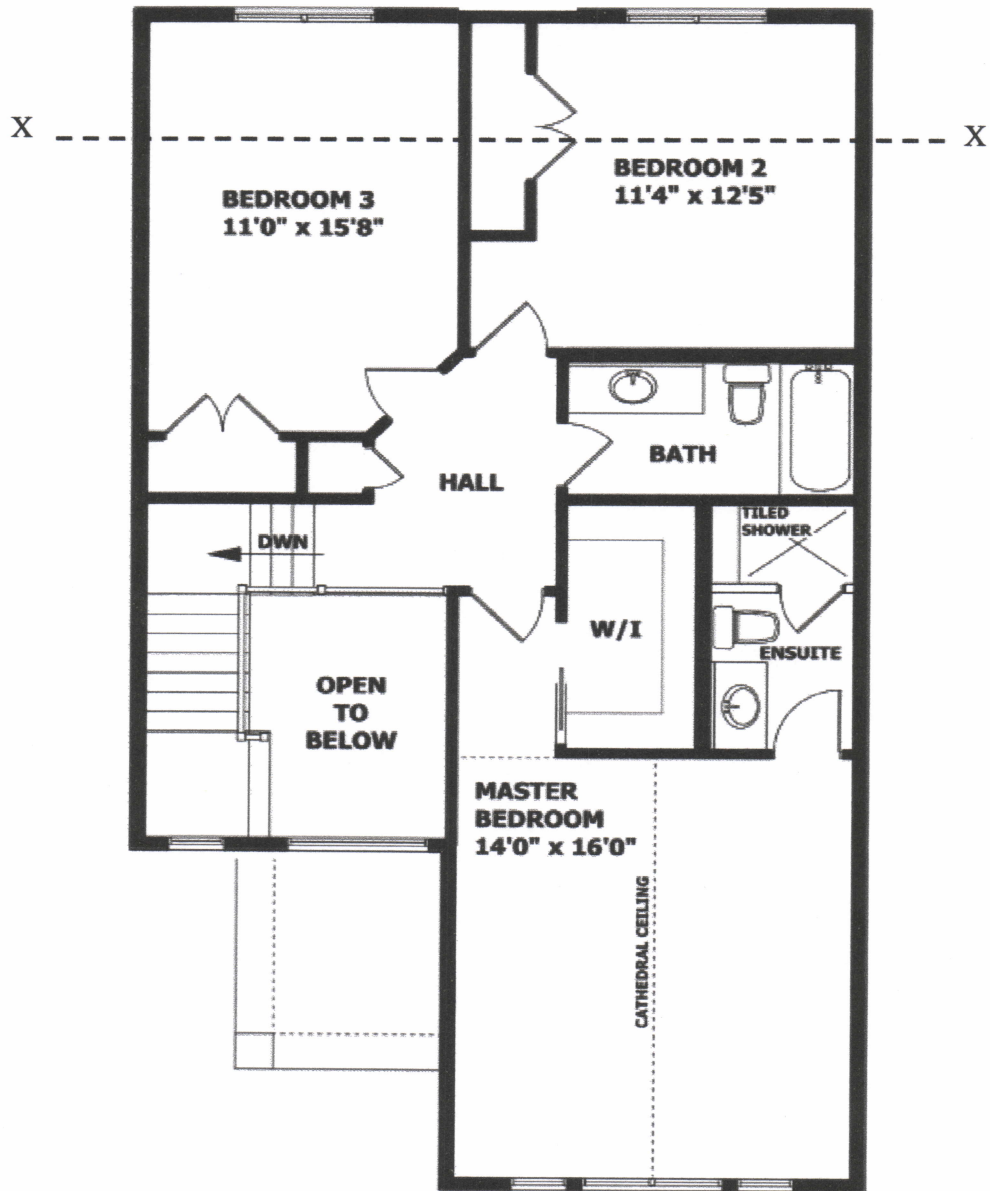
- (a) Determine the positive and negative moments for slab B-C/2-3. (5 marks)
- (b) Design the flexural reinforcement required at mid span by assuming that the bar size is 10mm. Determine the minimum and maximum reinforcement area. (12 marks)
- (c) Check the deflection for the slab panel. (8 marks)

-END OF QUESTIONS-

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1' = 0.305 m

FIGURE Q1

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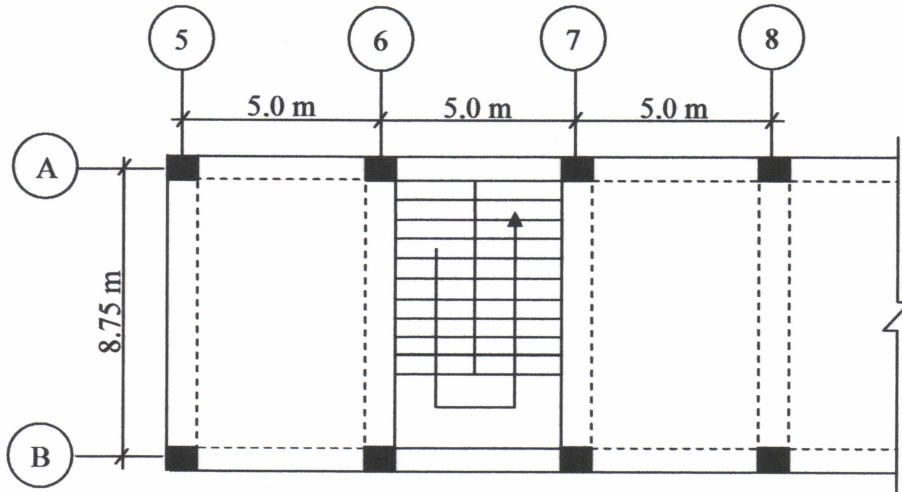


FIGURE Q2

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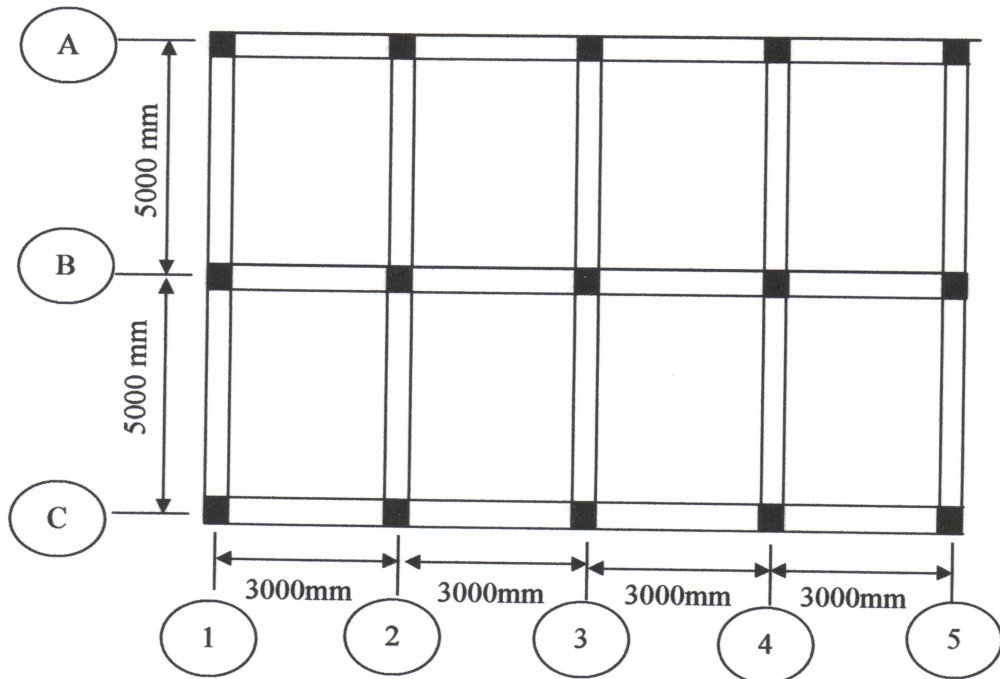


FIGURE Q3

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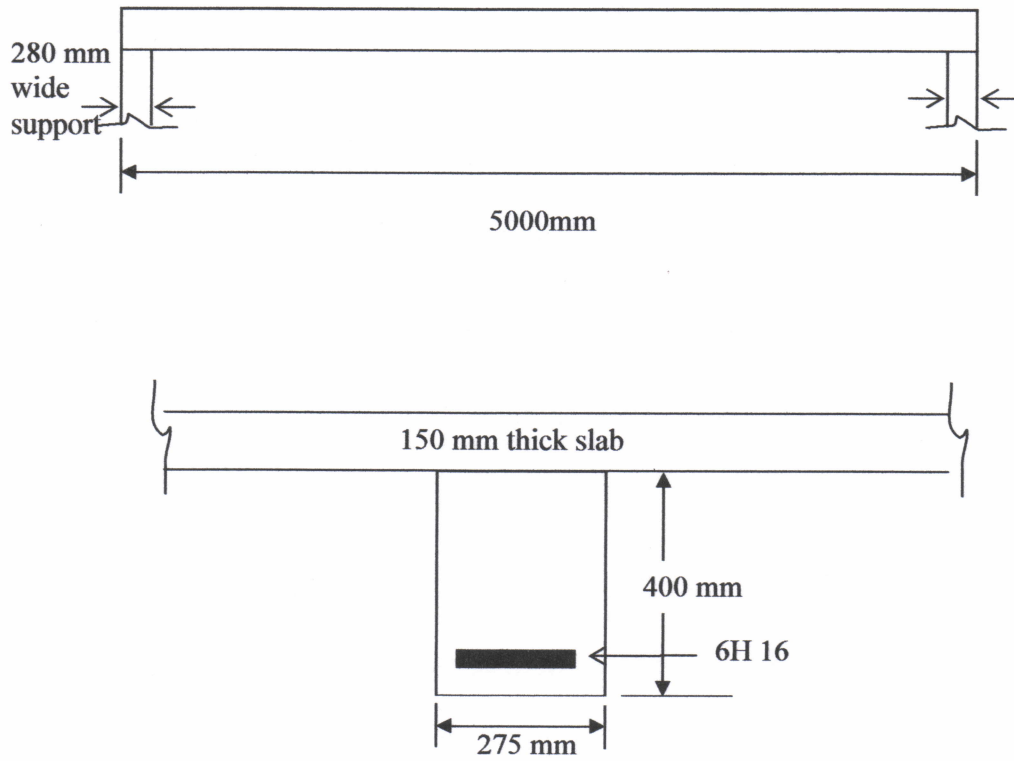


FIGURE Q4

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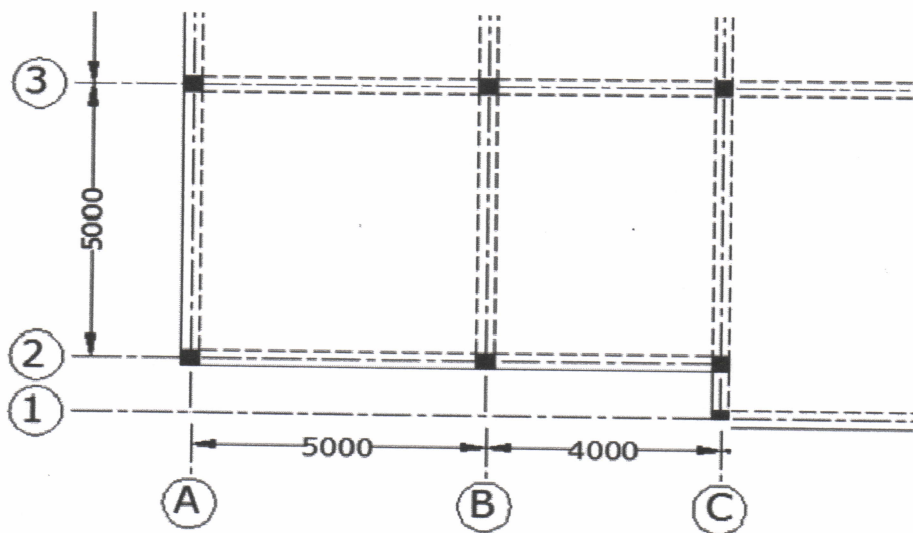
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Unit is in mm

FIGURE Q5

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FORMULA

$$A_s' = \frac{(K - K_{bal})f_{ck}bd^2}{0.87f_{yk}(d - d')} \quad \text{if } \frac{d'}{x} > 0.38$$

$$A_s' = \frac{(K - K_{bal})f_{ck}bd^2}{f_{sc}(d - d')} \quad \text{if } \frac{d'}{x} > 0.38$$

$$f_{sc} = 700 \left(1 - \frac{d'}{x}\right)$$

$$A_s = \frac{K_{bal}f_{ck}bd^2}{0.87f_{yk}(d - d')} + A_s' \left(\frac{f_{sc}}{0.87f_{yk}}\right)$$

$$V_{Rd,max} = \frac{0.36b_wdf_{ck}(1 - f_{ck}/250)}{\cot\theta + \tan\theta}$$

$$\theta = 0.5 \sin^{-1} \left(\frac{V_{Ed}}{0.18bdf_{ck}(1 - f_{ck}/250)} \right)$$

$$\frac{A_{sw}}{s} = \frac{V_{Ed}}{0.78f_{yk}d \cot\theta}$$

$$\frac{A_{sw}}{s} = \frac{0.08b_w\sqrt{f_{ck}}}{0.78f_{yk}d \cot\theta}$$

$$f_s = \frac{f_{yk}}{1.15} \left[\frac{G_k + 0.3Q_k}{1.35G_k + 1.5Q_k} \right] \frac{1}{\delta} \frac{A_{s,req}}{A_{s,prov}}$$

$$M_f = (0.567f_{ck}bh_f)(d - h_f/2)$$

$$M_{bal} = \beta_f f_{ck} b_{eff} d^2$$

$$\frac{M_{bal}}{f_{ck} b_{eff} d^2} = 0.167 \frac{b_w}{b_{eff}} + 0.567 \frac{h_f}{d} \left(1 - \frac{b_w}{b_{eff}}\right) \left(1 - \frac{h_f}{2d}\right)$$

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FORMULA

$$A_s = \frac{M}{0.87 f_{yk} z} \quad \text{if } M < M_f$$

$$A_s = \frac{M + 0.1 f_{ck} b_w d [0.36d - h_f]}{0.87 f_{yk} (d - 0.5h_f)} \quad \text{if } M < M_{bal}$$

$$A_s = \frac{0.2 f_{ck} b_w d + 0.567 f_{ck} h_f (b_{eff} - b_w)}{0.87 f_{yk}} + A_s' \quad \text{if } M > M_{bal}$$

$$A_s' = \frac{M - M_{bal}}{0.87 f_{yk} (d - d')} \quad \text{if } M > M_{bal}$$

$$V_{Rd,c} = [0.12k(100\rho_1 f_{ck})^{1/3}] b_w d$$

$$V_{min} = [0.035k^{3/2} f_{ck}^{1/2}] b_w d$$

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Table 1: Minimum dimensions and axis distances for simply supported beams made with reinforced and prestressed concrete (Source: BS EN 1992 -1-2)

| Standard fire resistance | Minimum dimensions (mm) | | | | | | |
|--------------------------|--|-----------|------------|------------|---------------------|----------|----------|
| | Possible combinations of a and b_{min} where a is the average axis distance and b_{min} is the width of beam | | | | Web thickness b_w | | |
| | | | | | Class WA | Class WB | Class WC |
| 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 |
| R 30 | $b_{min}= 80$ $a = 25$ | 120 20 | 160 15* | 200 15* | 80 | 80 | 80 |
| R 60 | $b_{min}= 120$ $a = 40$ | 160 35 | 200 30 | 300 25 | 100 | 80 | 100 |
| R 90 | $b_{min}= 150$ $a = 55$ | 200 45 | 300 40 | 400 35 | 110 | 100 | 100 |
| R 120 | $b_{min}= 200$ $a = 65$ | 240 60 | 300 55 | 500 50 | 130 | 120 | 120 |
| R 180 | $b_{min}= 240$ $a = 80$ | 300 70 | 400 65 | 600 60 | 150 | 150 | 140 |
| R 240 | $b_{min}= 280$ $a = 90$ | 350 80 | 500 75 | 700 70 | 170 | 170 | 160 |

$a_{sd} = a + 10\text{mm}$ (see note below)

For prestressed beams the increase of axis distance according to 5.2(5) should be noted.

a_{sd} is the axis distance to the side of beam for the corner bars (or tendon or wire) of beams with only one layer of reinforcement. For values of b_{min} greater than that given in Column 4 no increase of a_{sd} is required.

* Normally the cover required by EN 1992-1-1 will control.

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Table 2: Minimum dimensions and axis distances for reinforced and prestressed concrete simply supported one-way and two-way solid slabs (Source: BS EN 1992 -1-2)

- (1) Table 5.8 provides minimum values of axis distance to the soffit of simply supported slabs for standard fire resistance of R 30 and to R 40,
- (2) In two-way spanning slabs, a denotes the axis distance of the reinforcement in the lower layer.

| Standard fire resistance | Minimum dimensions (mm) | | | |
|--------------------------|---------------------------|-------------------|--------------------|---------------------|
| | slab thickness h_s (mm) | axis-distance a | | |
| | | one way | two way: | |
| | | | $l_y/l_x \leq 1,5$ | $1,5 < l_y/l_x < 2$ |
| 1 | 2 | 3 | 4 | 5 |
| REI 30 | 60 | 10* | 10* | 10* |
| REI 60 | 80 | 20 | 10* | 15* |
| REI 90 | 100 | 30 | 15* | 20 |
| REI 120 | 120 | 40 | 20 | 25 |
| REI 180 | 150 | 55 | 30 | 40 |
| REI 240 | 175 | 65 | 40 | 50 |

l_x and l_y are the spans of a two-way slab (two directions at right angles) where l_y is the longer span.

For prestressed slabs the increase of axis distance according to 5.2(5) should be noted.

The axis distance a in Column 4 and 5 for two-way slabs relate to slabs supported at all four edges. Otherwise, they should be treated as one-way spanning slab.

* Normally the cover required by EN 1992-1-1 will control.

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**Table 3: Design ultimate bending moments and shear forces
 (Source: BS 8110 -1: 1997)**

| | At outer support | Near middle of end span | At first interior support | At middle of interior spans | At interior supports |
|--------|------------------|-------------------------|---------------------------|-----------------------------|----------------------|
| Moment | 0 | $0.09Fl$ | $-0.11Fl$ | $0.07Fl$ | $-0.08Fl$ |
| Shear | $0.45F$ | - | $0.6F$ | - | $0.55F$ |

NOTE: l is the effective span;

F is the total design ultimate load ($1.35G_k + 1.5 Q_k$)

No redistribution of the moment calculated from this table should be made.

**Table 4: Ultimate bending moment and shear force in one-way spanning slabs
 (Source: BS 8110 -1: 1997)**

| | End support/slab connection | | | | At first interior support | Middle interior spans | Interior supports |
|--------|-----------------------------|-------------------------|------------------|-------------------------|---------------------------|-----------------------|-------------------|
| | Simple | | Continuous | | | | |
| | At outer support | Near middle of end span | At outer support | Near middle of end span | | | |
| Moment | 0 | $0.086Fl$ | $-0.04Fl$ | $0.075Fl$ | $-0.086Fl$ | $0.063Fl$ | $-0.063Fl$ |
| Shear | $0.45F$ | - | $0.46F$ | - | $0.6F$ | - | $0.5F$ |

NOTE: l is the effective span;

F is the total design ultimate load ($1.35G_k + 1.5 Q_k$)

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Table 5: Shear force coefficient for uniformly loaded rectangular panels supported on four sides with provision for torsion at corners

Table 3.15 — Shear force coefficient for uniformly loaded rectangular panels supported on four sides with provision for torsion at corners

| Type of panel and location | β_{cr} for values of l_y/l_x | | | | | | | | β_{cr} |
|---|--------------------------------------|------|------|------|------|------|------|------|--------------|
| | 1.0 | 1.1 | 1.2 | 1.3 | 1.4 | 1.5 | 1.75 | 2.0 | |
| Four edges continuous | | | | | | | | | |
| Continuous edge | 0.33 | 0.36 | 0.39 | 0.41 | 0.43 | 0.45 | 0.48 | 0.50 | 0.33 |
| One short edge discontinuous | | | | | | | | | |
| Continuous edge | 0.36 | 0.39 | 0.42 | 0.44 | 0.45 | 0.47 | 0.50 | 0.52 | 0.36 |
| Discontinuous edge | — | — | — | — | — | — | — | — | 0.24 |
| One long edge discontinuous | | | | | | | | | |
| Continuous edge | 0.36 | 0.40 | 0.44 | 0.47 | 0.49 | 0.51 | 0.55 | 0.59 | 0.36 |
| Discontinuous edge | 0.24 | 0.27 | 0.29 | 0.31 | 0.32 | 0.34 | 0.36 | 0.38 | — |
| Two adjacent edges discontinuous | | | | | | | | | |
| Continuous edge | 0.40 | 0.44 | 0.47 | 0.50 | 0.52 | 0.54 | 0.57 | 0.60 | 0.40 |
| Discontinuous edge | 0.26 | 0.29 | 0.31 | 0.33 | 0.34 | 0.35 | 0.38 | 0.40 | 0.26 |
| Two short edges discontinuous | | | | | | | | | |
| Continuous edge | 0.40 | 0.43 | 0.45 | 0.47 | 0.48 | 0.49 | 0.52 | 0.54 | — |
| Discontinuous edge | — | — | — | — | — | — | — | — | 0.26 |
| Two long edges discontinuous | | | | | | | | | |
| Continuous edge | — | — | — | — | — | — | — | — | 0.40 |
| Discontinuous edge | 0.26 | 0.30 | 0.33 | 0.36 | 0.38 | 0.40 | 0.44 | 0.47 | — |
| Three edges discontinuous (one long edge discontinuous) | | | | | | | | | |
| Continuous edge | 0.45 | 0.48 | 0.51 | 0.53 | 0.55 | 0.57 | 0.60 | 0.63 | — |
| Discontinuous edge | 0.30 | 0.32 | 0.34 | 0.35 | 0.36 | 0.37 | 0.39 | 0.41 | 0.29 |
| Three edges discontinuous (one short edge discontinuous) | | | | | | | | | |
| Continuous edge | — | — | — | — | — | — | — | — | 0.45 |
| Discontinuous edge | 0.29 | 0.33 | 0.36 | 0.38 | 0.40 | 0.42 | 0.45 | 0.48 | 0.30 |
| Four edges discontinuous | | | | | | | | | |
| Discontinuous edge | 0.33 | 0.36 | 0.39 | 0.41 | 0.43 | 0.45 | 0.48 | 0.50 | 0.33 |

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Table 6: Bending moment coefficient for rectangular panels supported on four sides with provision for torsion at corners

Table 3.14 — Bending moment coefficients for rectangular panels supported on four sides with provision for torsion at corners

| Type of panel and moments considered | Short span coefficients, β_m | | | | | | | | Long span coefficients, β_{lx} for all values of l_y/l_x |
|--|------------------------------------|-------|-------|-------|-------|-------|-------|-------|--|
| | Values of l_y/l_x | | | | | | | | |
| | 1.0 | 1.1 | 1.2 | 1.3 | 1.4 | 1.5 | 1.75 | 2.0 | |
| Interior panels | | | | | | | | | |
| Negative moment at continuous edge | 0.031 | 0.037 | 0.042 | 0.046 | 0.050 | 0.053 | 0.059 | 0.063 | 0.032 |
| Positive moment at mid-span | 0.024 | 0.028 | 0.032 | 0.035 | 0.037 | 0.040 | 0.044 | 0.048 | 0.024 |
| One short edge discontinuous | | | | | | | | | |
| Negative moment at continuous edge | 0.039 | 0.044 | 0.048 | 0.052 | 0.055 | 0.058 | 0.063 | 0.067 | 0.037 |
| Positive moment at mid-span | 0.029 | 0.033 | 0.036 | 0.039 | 0.041 | 0.043 | 0.047 | 0.050 | 0.028 |
| One long edge discontinuous | | | | | | | | | |
| Negative moment at continuous edge | 0.039 | 0.049 | 0.056 | 0.062 | 0.068 | 0.073 | 0.082 | 0.089 | 0.037 |
| Positive moment at mid-span | 0.030 | 0.036 | 0.042 | 0.047 | 0.051 | 0.055 | 0.062 | 0.067 | 0.028 |
| Two adjacent edges discontinuous | | | | | | | | | |
| Negative moment at continuous edge | 0.047 | 0.056 | 0.063 | 0.069 | 0.074 | 0.078 | 0.087 | 0.093 | 0.045 |
| Positive moment at mid-span | 0.036 | 0.042 | 0.047 | 0.051 | 0.055 | 0.059 | 0.065 | 0.070 | 0.034 |
| Two short edges discontinuous | | | | | | | | | |
| Negative moment at continuous edge | 0.046 | 0.050 | 0.054 | 0.057 | 0.060 | 0.062 | 0.067 | 0.070 | — |
| Positive moment at mid-span | 0.034 | 0.038 | 0.040 | 0.043 | 0.045 | 0.047 | 0.050 | 0.053 | 0.034 |
| Two long edges discontinuous | | | | | | | | | |
| Negative moment at continuous edge | — | — | — | — | — | — | — | — | 0.045 |
| Positive moment at mid-span | 0.034 | 0.046 | 0.056 | 0.065 | 0.072 | 0.078 | 0.091 | 0.100 | 0.034 |
| Three edges discontinuous (one long edge continuous) | | | | | | | | | |
| Negative moment at continuous edge | 0.057 | 0.065 | 0.071 | 0.076 | 0.081 | 0.084 | 0.092 | 0.098 | — |
| Positive moment at mid-span | 0.043 | 0.048 | 0.053 | 0.057 | 0.060 | 0.063 | 0.069 | 0.074 | 0.044 |
| Three edges discontinuous (one short edge continuous) | | | | | | | | | |
| Negative moment at continuous edge | — | — | — | — | — | — | — | — | 0.058 |
| Positive moment at mid-span | 0.042 | 0.054 | 0.063 | 0.071 | 0.078 | 0.084 | 0.096 | 0.105 | 0.044 |
| Four edges discontinuous | | | | | | | | | |
| Positive moment at mid-span | 0.055 | 0.065 | 0.074 | 0.081 | 0.087 | 0.092 | 0.103 | 0.111 | 0.056 |

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