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UNIVERSITI TUN HUSSEIN ONN MALAYSIA

**FINAL EXAMINATION
SEMESTER II
SESSION 2015/2016**

COURSE NAME : PRESTRESSED CONCRETE
DESIGN

COURSE CODE : BFS 40303

PROGRAMME CODE : BFF

EXAMINATION DATE : JUNE/JULY 2016

DURATION : 3 HOURS

INSTRUCTION : ANSWER **FOUR (4)** QUESTIONS
ONLY

THIS QUESTION PAPER CONSISTS OF SEVEN (7) PAGES

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- Q1** (a) Illustrate the usual stages in producing a post-tensioned member. (6 marks)
- (b) A rectangular concrete beam of cross-section 300 mm deep and 200 mm wide is prestressed by means of 15 wires of 5 mm diameter located 65 mm from the bottom of the beam and 3 wires of diameter of 5 mm, 25 mm from the top. Assume the effective prestress in the steel is 840 N/mm^2 . The beam is supporting its own weight over a span of 6 m and uniformly distributed live load of 6 kN/m is imposed. The density of concrete is 24 kN/m^3 .
- (i) Develop the stresses at the extreme fibres of the mid-span section. (12 marks)
- (ii) Evaluate the maximum working stress in concrete. (7 marks)
- Q2** (a) Distinguish between concentric and eccentric tendons by indicating their applications. (10 marks)
- (b) A prestressed concrete pile, 250 mm square, contains 60 pre-tension wires that are initially tensioned on the prestressing bed with a total force of 300kN. Given the following data :
- $E_s: 210 \text{ kN/mm}^2$
 $E_c: 32 \text{ kN/mm}^2$
Shortening due to creep: $30 \times 10^{-6} \text{ mm/mm per N/mm}^2$ of stress
Total Shrinkage: 200×10^{-6} per unit length
Relaxation of Steel stress : 5%
- Evaluate the final stress in concrete and the percentage losses of stress in steel. (15 marks)
- Q3** (a) Describe the significance of minimum prestressing force, corresponding maximum eccentricity in the design of prestressing concrete section. (5 marks)
- (b) A prestressed concrete beam supports a live load of 5 kN/m along a simply supported span of 10 m. The beam has an I-section as shown in **FIGURE Q3**. The beam is to be prestressed by an effective prestressing force of 240 kN at a suitable eccentricity such that the resultant stresses at the soffit of the beam at the mid-span is zero. Use density of concrete = 24 kN/m^3

- (i) Determine the eccentricity required for the prestressed concrete beam
(10 marks)
- (ii) If the tendon is concentric, generate the magnitude of the prestressing force for the resultant stress to be zero at the bottom fibre at the central span section.
(10 marks)

Q4 A post-tensioned prestressed beam of rectangular section 250 mm wide is to be designed for an imposed load of 12 kN/m, uniformly distributed on a span of 12 m. The stress in the concrete must not exceed 17 N/mm² in compression and 1.4 N/mm² in tension at any time and the loss of prestress may be assumed to be 15%.

- (a) Determine the minimum depth of the beam.
(5 marks)
- (b) Calculate the minimum prestressing force and corresponding eccentricity.
(10 marks)
- (c) Construct the Magnel diagram and evaluate the minimum prestressing force corresponding to eccentricity.
(10 marks)

Q5 The cross section of a prestressed concrete composite beam is shown in **FIGURE Q5**. The beam is to span 20 m on simple supports and carry a characteristic imposed dead load of 4.5 kN/m and a characteristic imposed live load of 5 kN/m. The method of construction used was unshored. The following information is given:

Precast beam (Class 1)

$$f_{ci} = 30 \text{ MPa}; f_{cu} = 50 \text{ MPa}; E_{ci} = 27 \text{ GPa}; E_c = 32 \text{ GPa}; A_c = 324,400 \text{ mm}^2;$$

$$I_g = 38.1 \times 10^9 \text{ mm}^4; (dc)_{min} = 120 \text{ mm}; \eta = 0.8$$

Cast-in-place slab

$$f_{cu} = 30 \text{ MPa}; E_c = 27 \text{ GPa}; (\sigma_{cs})_{slab} = 10 \text{ MPa}$$

Composite section

$$A_{cc} = 552,250 \text{ mm}^2; I_{gc} = 90 \times 10^9 \text{ mm}^4; Y_{bc} = 711 \text{ mm}; Z_{tc} = 205 \times 10^6 \text{ mm}^3;$$

$$Z'_{tc} = 311 \times 10^6 \text{ mm}^3; Z_{bc} = 127 \times 10^6 \text{ mm}^3$$

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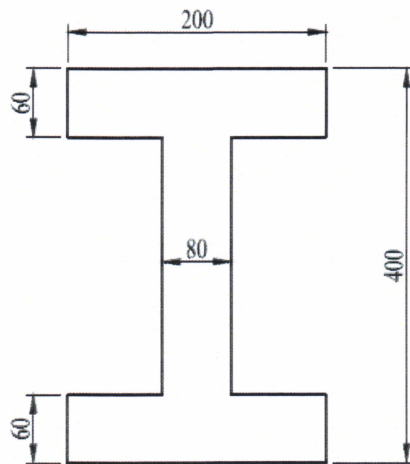
- (a) Justify the adequacy of 150 mm thickness of the slab. (10 marks)
- (b) Develop the minimum initial prestressing force necessary at mid-span using direct solution approach and graphical construction. (15 marks)

- END OF QUESTIONS -

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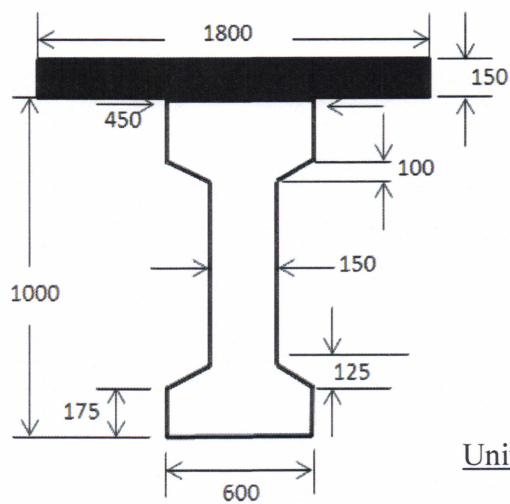
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Unit in mm

FIGURE Q3



Unit in mm

FIGURE Q5

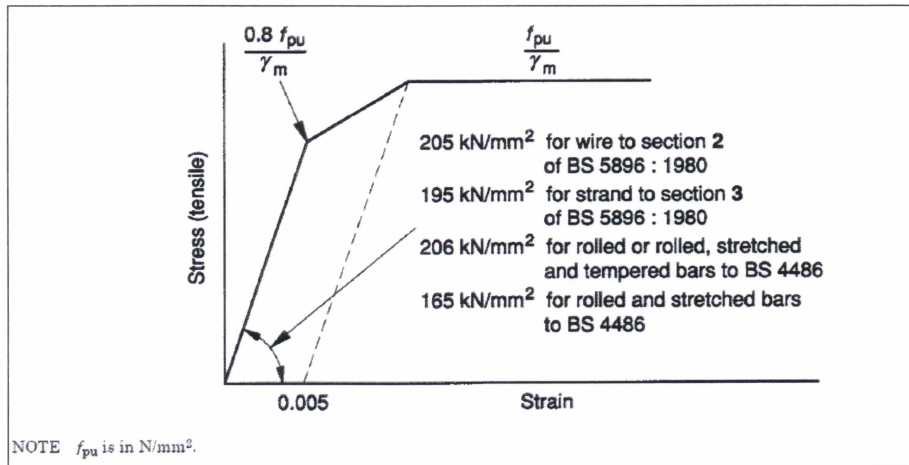
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APPENDIX

(A) Stress-Strain Curve of Prestressing Tendons



(B) Basic Inequalities

$$\frac{\alpha P_i}{A} - \frac{\alpha P_i e}{Z_t} + \frac{M_i}{Z_t} \geq f_{tt}$$

$$\frac{\alpha P_i}{A} + \frac{\alpha P_i e}{Z_b} - \frac{M_i}{Z_b} \geq f_{ct}$$

$$\frac{\beta P_i}{A} - \frac{\beta P_i e}{Z_t} + \frac{M_s}{Z_t} \geq f_{cs}$$

$$\frac{\beta P_i}{A} + \frac{\beta P_i e}{Z_b} - \frac{M_s}{Z_b} \geq f_{ts}$$

$$Z_t \geq \frac{M_{max} - \eta M_{min}}{f_{cs} - \eta f_{tt}}$$

$$Z_b \geq \frac{M_{max} - \eta M_{min}}{\eta f_{ct} - f_{ts}}$$

$$P_i \geq \frac{Z_t f_{tt} - M_i}{\left(\frac{Z_t}{A} - e\right)}$$

$$P_i \leq \frac{Z_b f_{ct} + M_i}{\left(\frac{Z_b}{A} + e\right)}$$

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$$P_i \leq \frac{Z_t f_{cs} - M_s}{\beta \left(\frac{Z_t}{A} - e \right)}$$

$$P_i \geq \frac{Z_b f_{ts} + M_s}{\beta \left(\frac{Z_b}{A} + e \right)}$$

(C) Strain Compatibility Analysis

$$\varepsilon_{pb} = \varepsilon_{pe} + \varepsilon_{pa}$$

$$\varepsilon_{pe} = \frac{\beta P}{A_{ps} E_s}$$

$$\varepsilon_{pa} = \beta_1 \varepsilon_e + \beta_2 \varepsilon_u$$

Where;

β_1 and β_2 = bond coefficients

β_1 and β_2 = 1.0 for fully bonded tendon

$\varepsilon_e = \frac{1}{E_c}$ x stress in concrete at tendon level due to effective prestress.

$$\varepsilon_e = \frac{\beta}{E_c} \left[\frac{P}{A} + \frac{Pe^2}{I} \right]$$

$$\varepsilon_u = \frac{d-x}{x} \varepsilon_{cu}$$

where $\varepsilon_{cu} = 0.0035$

$$\varepsilon_{pb} = \varepsilon_{pe} + \beta_1 \varepsilon_e + \beta_2 \varepsilon_{cu} \left(\frac{d-x}{x} \right)$$

$$x = \left[\frac{\beta_2 \varepsilon_{cu}}{\beta_2 \varepsilon_{cu} + \varepsilon_{pb} - \varepsilon_{pe} - \beta_1 \varepsilon_e} \right] d$$