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UNIVERSITI TUN HUSSEIN ONN MALAYSIA

**FINAL EXAMINATION
SEMESTER I
SESSION 2012/2013**

COURSE NAME : COASTAL & HARBOUR
ENGINEERING

COURSE CODE : BFW 4033 / BFW 40303

PROGRAMME : 4 BFF

EXAMINATION DATE : DECEMBER 2012/JANUARY 2013

DURATION : 3 HOURS

INSTRUCTIONS : ANSWER FIVE (5) QUESTIONS

THIS QUESTION PAPER CONSISTS OF FOURTEEN (14) PAGES

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- Q1** (a) State the following
- (i) Length of Malaysia coastline (2 marks)
 - (ii) **TWO (2)** common types of coast found along Malaysia shore (2 marks)
- (b) Discuss **FOUR (4)** problems faced by Malaysia coasts. (16 marks)
-
- Q2** (a) Provide **THREE (3)** of the following main natural forces which are involved in the generation of ocean waves
- (i) Disturbing force (3 marks)
 - (ii) Restoring force (3 marks)
- (b) A wave with height 3 m and period 7 s propagates shoreward from a depth $d = 150$ m to a depth $d = 5$ m. Find
- (i) Wave length and celerity at depths 150 m and 5 m (9 marks)
 - (ii) Maximum horizontal and vertical local velocities of the surface at depth 5 m (5 marks)
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- Q3** (a) With the aid of sketches, briefly explain the wave processes of
- (i) Reflection (3 marks)
 - (ii) Refraction (3 marks)
 - (iii) Diffraction (3 marks)
- (b) A 2.5 m-high deepwater wave is propagating towards a 1:10 beach, with its crest making an angle of $\alpha_0 = 30^\circ$ with the shoreline. As the wave moves into shallower water, its speed reduces from 15 m/s to 5 m/s. Compute the wave height and depth at breaking. (11 marks)

- Q4** (a) Describe **THREE (3)** factors which influence the height and period of wind-generated waves. (6 marks)
- (b) **Figure Q4** shows the ocean surface elevation recorded during an event. Determine
 (i) Significant wave height H_s
 (ii) Maximum wave height H_{\max}
 (iii) Average of the highest 10% of the wave height H_{10} (8 marks)
- (c) Based on the coastal camp experience, describe how the wave celerity and wave frequency are determined on site. (6 marks)
- Q5** A rock revetment with slope 1:2.5 and crest level 4.5 m CD is to be built on a beach with foreshore gradient of 1:100. The significant wave height is $H_s = 3.0$ m, peak wave period $T_p = 10$ s, and design water level DWL = 3.5 m CD.
- (a) Determine whether the overtopping performance of the structure is acceptable to justify its use to protect a paved promenade based on **Figure Q5**. (10 marks)
- (b) Propose a modification that should be made to the revetment to ensure the paved promenade is safe for use. (3 marks)
- (c) Determine suitable size of rock armours to be placed on the slope of the structure assuming 'no damage' level. Assume seawater density $\rho_w = 1025$ kg/m³, rock armour density $\rho_r = 2700$ kg/m³, and $K_D = 3.0$. (7 marks)
- Q6** (a) Briefly discuss **EIGHT (8)** considerations to be made in accomplishing an economically desired coastal protection design. (12 marks)
- (b) Estimate the volume of fill material V required to nourish a beach with a berm height $B = 5.0$ m and width $Y = 50$ m where significant wave height $H_s = 3.5$ m. The depth of closure $H = 6.75H_s$, and the sedimentary parameters are $\sigma_{\phi_b} = 0.75$, $\sigma_{\phi_n} = 0.60$, $M_{\phi_b} = 2.30$, $M_{\phi_n} = 1.85$. Ignore the renourishment factor R_J . (8 marks)

TERJEMAHAN:

- S1** (a) Nyatakan yang berikut
- (i) Panjang garisan pantai Malaysia (2 markah)
 - (ii) **DUA (2)** jenis pantai umum yang boleh ditemui di sepanjang pantai Malaysia. (2 markah)
- (b) Bincangkan **EMPAT (4)** masalah yang dihadapi oleh kawasan pantai Malaysia. (16 markah)
-
- S2** (a) Berikan **TIGA (3)** daya-daya semulajadi utama yang mempengaruhi penjanaan ombak lautan
- (i) Daya gangguan (3 markah)
 - (ii) Daya pemulihan (3 markah)
- (b) Sebuah ombak dengan ketinggian 3 m dan tempoh 7 s bergerak ke arah pantai dari kedalaman $d = 150$ m ke kedalaman $d = 5$ m. Kira
- (i) Panjang dan laju ombak pada kedalaman 150 m dan kedalaman 5 m (9 markah)
 - (ii) Halaju tempatan maksimum mengufuk dan pugak di permukaan pada kedalaman 5 m. (5 markah)
-
- S3** (a) Berbantuan lakaran, huraikan secara ringkas proses-proses ombak berikut
- (i) Pemantulan (3 markah)
 - (ii) Pembiasan (3 markah)
 - (iii) Pembelauan (3 markah)
- (b) Satu ombak laut dalam setinggi 2.5 m bergerak ke sebuah pantai berkecerunan 1:10, dengan puncak ombak membentuk sudut $\alpha_0 = 30^\circ$ dengan garis pantai. Semasa ombak bergerak ke kedalaman yang lebih cetek, halaju rambatnya berkurangan dari 15 m/s ke 5 m/s. Kira tinggi ombak dan kedalaman ketika ombak pecah. (11 markah)

- S4** (a) Huraikan **TIGA (3)** faktor yang mempengaruhi tinggi dan tempoh ombak janaan angin. (6 markah)
- (b) **Rajah Q4** menunjukkan paras permukaan laut yang direkodkan bagi satu peristiwa. Tentukan
 (i) Tinggi ombak berkesan H_s
 (ii) Tinggi ombak maksimum H_{max}
 (iii) Tinggi purata bagi 10% ombak-ombak tertinggi H_{10} (8 markah)
- (c) Berdasarkan pengalaman kem pantai, huraikan bagaimana halaju rambat dan frekuensi ombak ditentukan di tapak. (6 markah)
- S5** Sebuah struktur pelindung pantai berbatu yang berkecerunan 1:2.5 dengan paras puncak 5.0 m CD akan dibina di pantai yang berkecerunan pantai 1:100. Tinggi ombak berkesan ialah $H_s = 3.0$ m, tempoh ombak puncak $T_p = 8$ s, dan paras air rekabentuk $DWL = 3.5$ m CD.
- (a) Tentukan samada prestasi struktur tersebut boleh diterima sebagai pelindung bagi laluan pejalan kaki berturap merujuk pada **Rajah S5**. (10 markah)
- (b) Nyatakan secara ringkas satu pengubahsuaian yang perlu dilakukan kepada struktur pelindung tersebut bagi menjamin keselamatan laluan pejalan kaki berturap tersebut. (3 markah)
- (c) Kira saiz pelindung batu yang sesuai diletakkan pada cerun struktur tersebut dengan andaian keadaan 'tiada kerosakan'. Andai ketumpatan air laut $\rho_w = 1025 \text{ kg/m}^3$, ketumpatan pelindung batu $\rho_r = 2700 \text{ kg/m}^3$, dan $K_D = 3.0$. (7 markah)
- S6** (a) Bincangkan secara ringkas **LAPAN (8)** pertimbangan yang perlu dibuat bagi mencapai rekabentuk perlindungan pantai yang ekonomi. (12 markah)
- (b) Kira isipadu bahan tambakan V yang diperlukan untuk pembajaan sebuah pantai dengan tinggi benteng $B = 5.0$ m dan lebar $Y = 50$ m, dimana tinggi ombak berkesan min $H_s = 3.5$ m. Kedalaman dasar (*depth of closure*) $H = 6.75H_s$, dan parameter sedimen ialah $\sigma_{\phi_b} = 0.75$, $\sigma_{\phi_n} = 0.60$, $M_{\phi_b} = 2.30$, $M_{\phi_n} = 1.85$. Abaikan pekali penambahan R_J . (8 markah)

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Supplementary equations

$$H_i = H_o K_s K_r$$

$$\text{where, } K_s = \sqrt{\frac{C_o}{C \left[1 + \frac{\left(\frac{4\pi d}{L} \right)}{\sinh\left(\frac{4\pi d}{L} \right)} \right]}}, \text{ and } K_r = \sqrt{\frac{\cos \alpha_o}{\cos \alpha}}$$

Unrefracted deepwater wave height $H'_o = H_o K_r$

$$\text{Snell's law : } \frac{\sin \alpha}{C} = \frac{\sin \alpha_o}{C_o}$$

$$T_m = 0.82 T_p$$

$$R^* = \frac{R_c}{T_m \sqrt{g H_s}}$$

$$Q^* = A e^{\left(\frac{-BR^*}{r} \right)}$$

$$q = Q^* T_m g H_s$$

$$M_{50} = \frac{\rho_r H_s^3}{K_D \cot \alpha \Delta^3}$$

$$D_{50} = \left(\frac{M_{50}}{\rho_r} \right)^{\frac{1}{3}}$$

$$\Delta = \frac{\rho_r}{\rho_w} - 1$$

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| Characteristic | Transitional water ($0.04 < d/L < 0.5$) | Deep water ($d/L_o \geq 0.5$) |
|----------------|--|---|
| Wave celerity | $C = \frac{L}{T} = \frac{gT}{2\pi} \tanh\left(\frac{2\pi d}{L}\right)$ | $C_o = \frac{L}{T} = \frac{gT}{2\pi}$ |
| Wave length | $L = \frac{gT^2}{2\pi} \tanh\left(\frac{2\pi d}{L}\right)$ | $L_o = \frac{gT^2}{2\pi}$ |
| Displacement | | |
| a. horizontal | $\xi = -\frac{H}{2} \frac{\cosh\left[2\pi \frac{(z+d)}{L}\right]}{\sinh\left(2\pi \frac{d}{L}\right)} \sin \theta$ | $\xi = -\frac{H}{2} e^{\frac{2\pi z}{L}} \sin \theta$ |
| b. vertical | $\zeta = \frac{H}{2} \frac{\sinh\left[2\pi \frac{(z+d)}{L}\right]}{\sinh\left(2\pi \frac{d}{L}\right)} \cos \theta$ | $\zeta = \frac{H}{2} e^{\frac{2\pi z}{L}} \cos \theta$ |
| Velocity | | |
| a. horizontal | $u = \frac{H}{2} \frac{gT}{L} \frac{\cosh\left[2\pi \frac{(z+d)}{L}\right]}{\cosh\left(2\pi \frac{d}{L}\right)} \cos \theta$ | $u = \frac{\pi H}{T} e^{\frac{2\pi z}{L}} \cos \theta$ |
| b. vertical | $w = \frac{H}{2} \frac{gT}{L} \frac{\sinh\left[2\pi \frac{(z+d)}{L}\right]}{\cosh\left(2\pi \frac{d}{L}\right)} \sin \theta$ | $w = \frac{\pi H}{T} e^{\frac{2\pi z}{L}} \sin \theta$ |
| Acceleration | | |
| a. horizontal | $a_x = \frac{g\pi H}{L} \frac{\cosh\left[2\pi \frac{(z+d)}{L}\right]}{\cosh\left(2\pi \frac{d}{L}\right)} \sin \theta$ | $a_x = 2H \left(\frac{\pi}{T}\right)^2 e^{\frac{2\pi z}{L}} \sin \theta$ |
| b. vertical | $a_z = -\frac{g\pi H}{L} \frac{\sinh\left[2\pi \frac{(z+d)}{L}\right]}{\cosh\left(2\pi \frac{d}{L}\right)} \cos \theta$ | $a_z = -2H \left(\frac{\pi}{T}\right)^2 e^{\frac{2\pi z}{L}} \cos \theta$ |

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Functions of d/L for even increments of d/L_0

| d/L_0 | d/L | $2\pi d/L$ | $\tanh 2\pi d/L$ | $\sinh 2\pi d/L$ | $\cosh 2\pi d/L$ |
|---------|---------|------------|------------------|------------------|------------------|
| 0.03000 | 0.07135 | 0.4483 | 0.4205 | 0.4634 | 1.1021 |
| 0.03100 | 0.07260 | 0.4562 | 0.4269 | 0.4721 | 1.1059 |
| 0.03200 | 0.07385 | 0.4640 | 0.4333 | 0.4808 | 1.1096 |
| 0.03300 | 0.07507 | 0.4717 | 0.4395 | 0.4894 | 1.1133 |
| 0.03400 | 0.07630 | 0.4794 | 0.4457 | 0.4980 | 1.1171 |
| 0.03500 | 0.07748 | 0.4868 | 0.4517 | 0.5064 | 1.1209 |
| 0.03600 | 0.07867 | 0.4943 | 0.4577 | 0.5147 | 1.1247 |
| 0.03700 | 0.07984 | 0.5017 | 0.4635 | 0.5230 | 1.1285 |
| 0.03800 | 0.08100 | 0.5090 | 0.4691 | 0.5312 | 1.1324 |
| 0.03900 | 0.08215 | 0.5162 | 0.4747 | 0.5394 | 1.1362 |
| 0.06000 | 0.1043 | 0.6553 | 0.5753 | 0.7033 | 1.2225 |
| 0.06100 | 0.1053 | 0.6616 | 0.5794 | 0.7110 | 1.2270 |
| 0.06200 | 0.1063 | 0.6678 | 0.5834 | 0.7187 | 1.2315 |
| 0.06300 | 0.1073 | 0.6739 | 0.5874 | 0.7256 | 1.2355 |
| 0.06400 | 0.1082 | 0.6799 | 0.5914 | 0.7335 | 1.2405 |
| 0.06500 | 0.1092 | 0.6860 | 0.5954 | 0.7411 | 1.2447 |
| 0.06600 | 0.1101 | 0.6920 | 0.5993 | 0.7486 | 1.2492 |
| 0.06700 | 0.1111 | 0.6981 | 0.6031 | 0.7561 | 1.2537 |
| 0.06800 | 0.1120 | 0.7037 | 0.6069 | 0.7633 | 1.2580 |
| 0.06900 | 0.1130 | 0.7099 | 0.6106 | 0.7711 | 1.2628 |
| 0.9000 | 0.9000 | 5.655 | 1.000 | 142.9 | 142.9 |
| 0.9100 | 0.9100 | 5.718 | 1.000 | 152.1 | 152.1 |
| 0.9200 | 0.9200 | 5.781 | 1.000 | 162.0 | 162.0 |
| 0.9300 | 0.9300 | 5.844 | 1.000 | 172.5 | 172.5 |
| 0.9400 | 0.9400 | 5.906 | 1.000 | 183.7 | 183.7 |
| 0.9500 | 0.9500 | 5.969 | 1.000 | 195.6 | 195.6 |
| 0.9600 | 0.9600 | 6.032 | 1.000 | 208.2 | 208.2 |
| 0.9700 | 0.9700 | 6.095 | 1.000 | 221.7 | 221.7 |
| 0.9800 | 0.9800 | 6.158 | 1.000 | 236.1 | 236.1 |
| 0.9900 | 0.9900 | 6.220 | 1.000 | 251.4 | 251.4 |

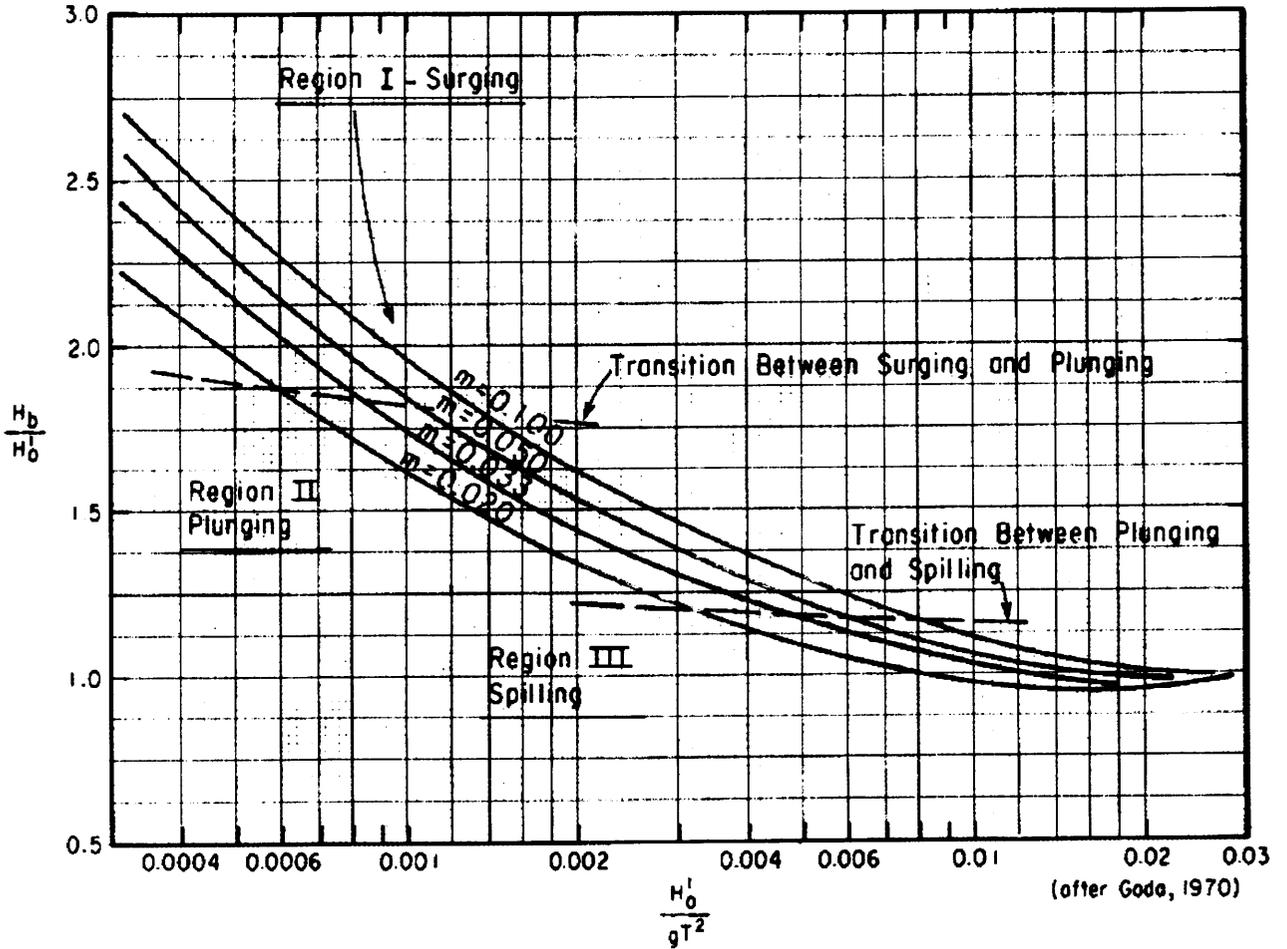
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Breaker height index versus deepwater wave steepness

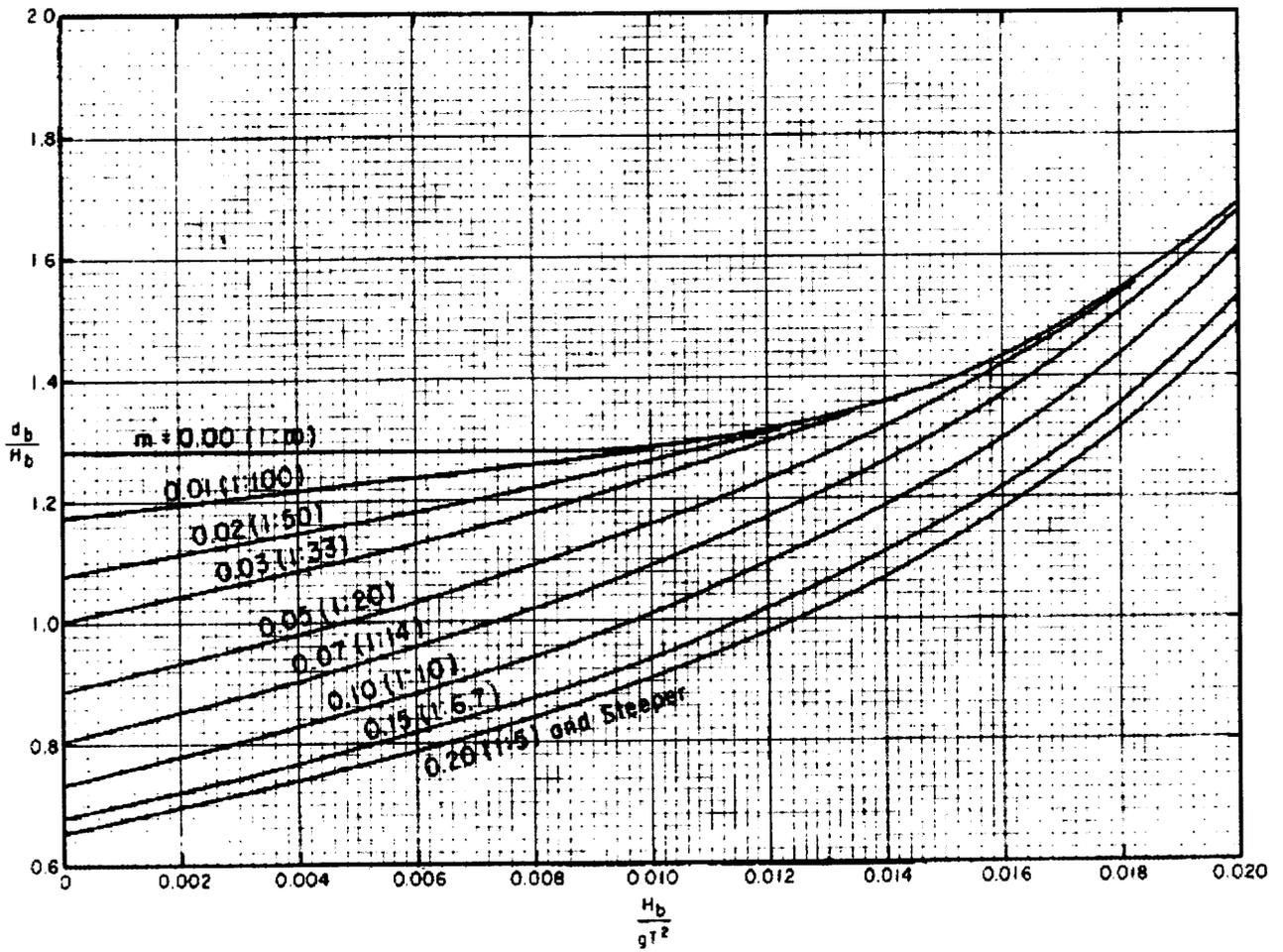
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Breaker index versus wave steepness

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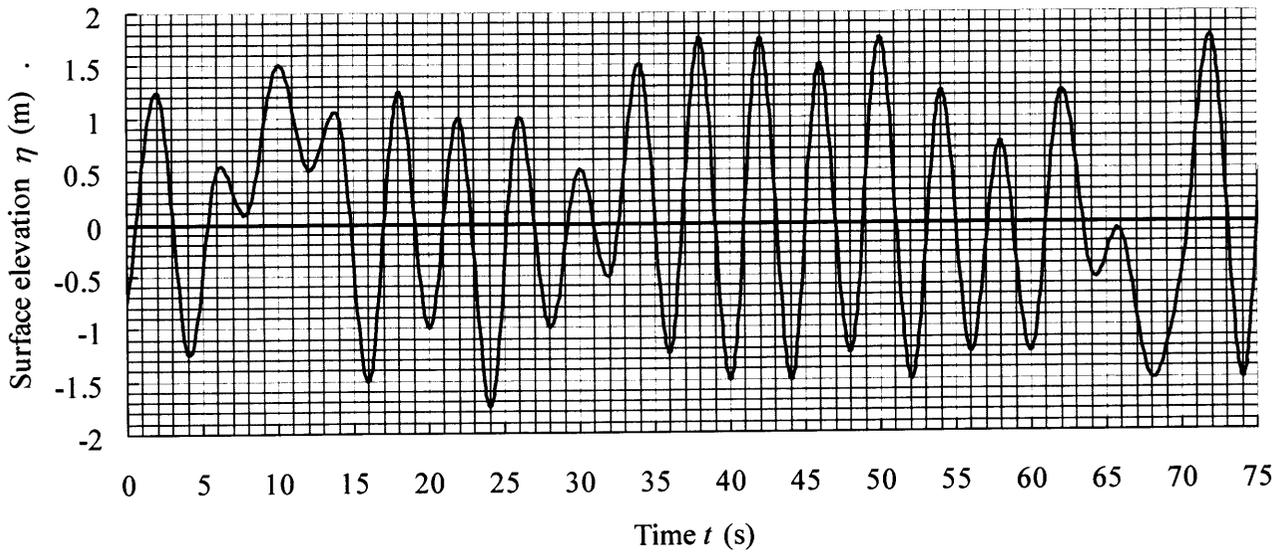


Figure Q4 / Rajah S4

Ratio of H_n/H_s from Rayleigh distribution

| n | H_n/H_s |
|-----|-----------|
| 1 | 1.67 |
| 2 | 1.56 |
| 5 | 1.40 |
| 10 | 1.27 |
| 20 | 1.12 |
| 50 | 0.89 |
| 100 | 0.63 |

Owen parameters

| Structure slope | A | B |
|-----------------|--------|-------|
| 1:1.5 | 0.0102 | 20.12 |
| 1:2.0 | 0.0125 | 22.06 |
| 1:2.5 | 0.0145 | 26.10 |
| 1:3.0 | 0.0163 | 31.90 |
| 1:3.5 | 0.0178 | 38.90 |
| 1:4.0 | 0.0192 | 46.96 |
| 1:4.5 | 0.0215 | 55.70 |
| 1:5.0 | 0.0250 | 65.20 |

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Mean overtopping discharge
 q
m³/s per m

q
litres/s per m

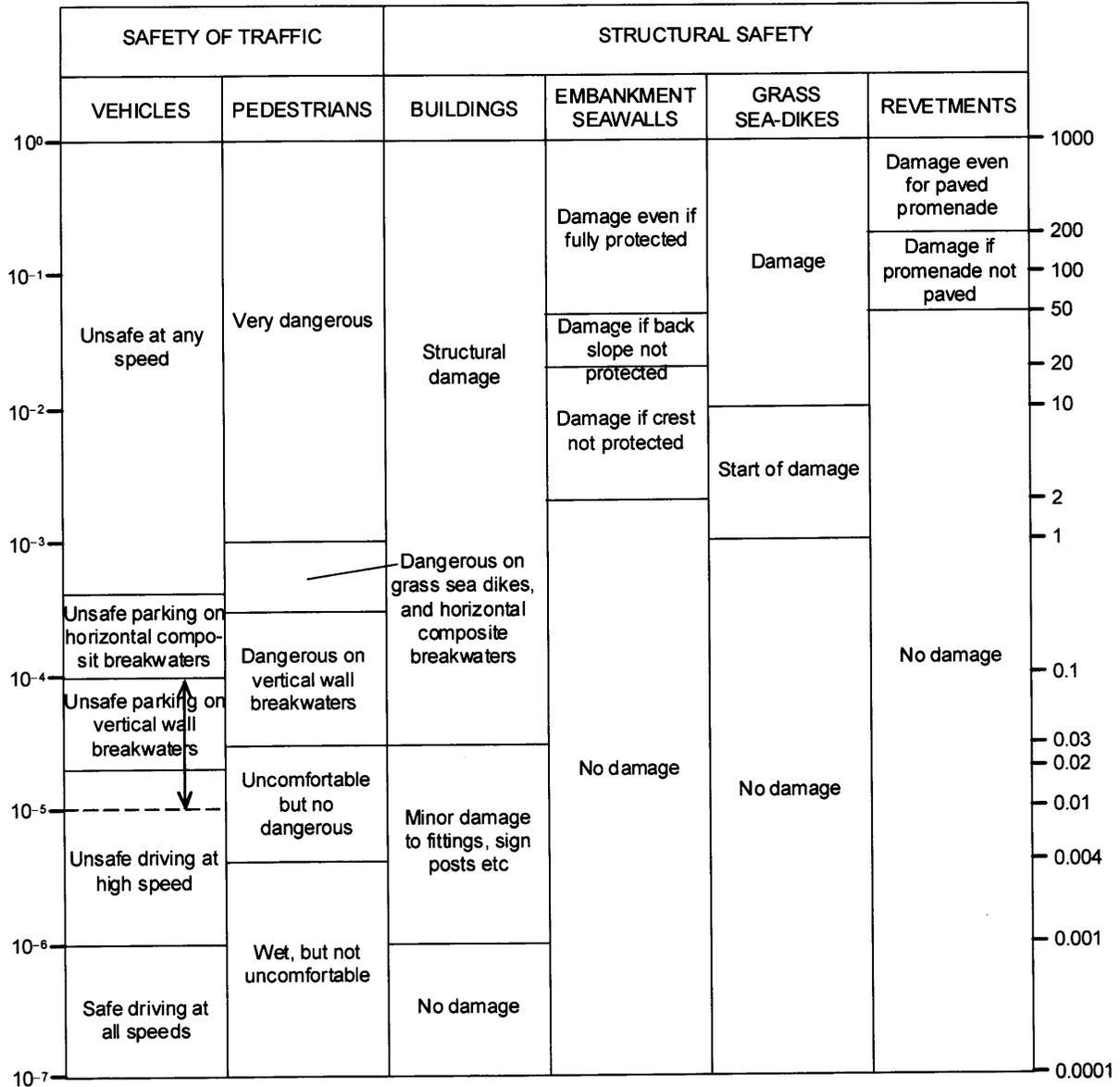


Figure Q5 / Rajah S5

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Roughness coefficient r

| Type of embankment/revetment | Roughness coefficient r |
|---|---------------------------|
| Smooth, impermeable | 1.0 |
| Stone blocks, pitched or mortared | 0.95 |
| Concrete blocks | 0.90 |
| Stone blocks, granite sets | 0.85 – 0.90 |
| Turf | 0.85 – 0.90 |
| Rough concrete | 0.85 |
| One layer of stone rubble on impermeable base | 0.80 |
| Stones set in cement, ragstone etc | 0.75 – 0.80 |
| Two or more layers of open rock armour | 0.50 – 0.60 |
| Open stone asphalt | 0.80 |
| Fully grouted stone | 0.60 – 0.80 |
| Partial grouted stone | 0.60 – 0.70 |

Relationship between M_ϕ and σ_ϕ of the native material and borrow material

| Case | Quadrant | Relationship of phi means | Relationship of phi standard deviations |
|------|----------|--|---|
| I | 1 | $M_{\phi b} > M_{\phi n}$ borrow material is finer than native material | $\sigma_{\phi b} > \sigma_{\phi n}$ borrow material is more poorly sorted than native material |
| II | 2 | $M_{\phi b} < M_{\phi n}$ borrow material is coarser than native material | |
| III | 3 | $M_{\phi b} < M_{\phi n}$ borrow material is coarser than native material | $\sigma_{\phi b} < \sigma_{\phi n}$ borrow material is better sorted than native material |
| IV | 4 | $M_{\phi b} > M_{\phi n}$ borrow material is finer than native material | |

