



UNIVERSITI TUN HUSSEIN ONN MALAYSIA

**FINAL EXAMINATION
SEMESTER II
SESSION 2017/2018**

COURSE NAME : **FOOD TECHNOLOGY
UNIT PROCESS 1**

COURSE CODE : **BWD 20903**

PROGRAMME CODE : **BWD**

EXAMINATION DATE : **JUNE / JULY 2018**

DURATION : **3 HOURS**

INSTRUCTION : **ANSWER ALL QUESTIONS**

THIS QUESTION PAPER CONSISTS OF SIX (6) PAGES

Q1 The operations carried out in the industrial processes may be performed in **THREE (3)** different ways; discontinuous/batch, continuous and semi-continuous/semi-batch. Analyse and compare the principles, advantages, and disadvantages of both operations as shown in **Figure Q1**.

(20 marks)

Q2 (a) 255 grams of water is heated from 25°C to 100°C. Calculate the amount of heat absorbed by the water. Given that the specific heat of water is $4.18 \text{ Jg}^{-1}\text{C}^{-1}$.

(5 marks)

(b) If air consists of 77% by weight of nitrogen and 23% by weight of oxygen. Calculate:

(i) the mean molecular weight of air

(ii) the mole fraction of oxygen

(iii) the concentration of oxygen in molm^{-3} and kgm^{-3} if the total pressure is 1.5 atmosphere and the temperature is 25°C.

(Molecular weight of nitrogen is 28 gmol^{-1} and oxygen is 32 gmol^{-1} ; R constant is $0.0821 \text{ m}^3\text{mol}^{-1} \text{ K}^{-1}$)

(15 marks)

Q3 (a) A heat exchanger is a device designed to efficiently transfer or exchange heat from one matter to another. 1 kgs^{-1} of air at 24°C is heated in a heat exchanger using saturated steam at 136 kNm^{-2} (1.36 bar). The flow rate of steam is 0.01 kgs^{-1} and the condensate (which is at 1.36 bar) leaves the heat exchanger at 84°C. If the specific heat capacity of air is 1.005 kJkg^{-1} , determine the exit temperature of air. Assume no heat is lost.

(Enthalpy of steam at 1.36 bar = 368 kJkg^{-1} ; enthalpy of water at 84°C and 1.36 bar = 2689 kJkg^{-1}).

(10 marks)

(b) Calculate the rate of convection heat loss to ambient air from the side walls of a cooking vessel in the form of a vertical cylinder 0.9 m in diameter and 1.2 m high. The outside of the vessel insulation, facing ambient air, is found to be at 49°C and the air temperature is 17°C.

(Viscosity = $1.9 \times 10^{-5} \text{ Nsm}^{-2}$, specific heat at constant pressure = $1.0 \text{ kJkg}^{-1}\text{C}^{-1}$, thermal conductivity = $0.025 \text{ Jm}^{-1}\text{s}^{-1}\text{C}^{-1}$, coefficient of thermal expansion = $1/308$, density = 1.12 kgm^{-3})

(10 marks)

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- Q4** (a) Compare and contrast between Newtonian and Bingham plastic types of fluid behaviour. (10 marks)
- (b) Shear-thinning products need to be shaken in a jar or mixed at high intensity in a mixer which may aid in their mixing. Distinguish what could have happened if the mixing or shearing action is stopped after a certain period of time. Use diagrams to support your answer. (10 marks)
- Q5** (a) There are several factors affecting convection rate. Identify **FIVE (5)** factors that could affect natural convection rate. (5 marks)
- (b) Calculate the steam requirement as you start to heat 50 kg of pea soup in a jacketed pan, if the initial temperature of the soup is 18°C and the steam used is at 100 kPa gauge. The pan has a heating surface of 1 m² and overall heat transfer coefficient is assumed to be 300 Jm⁻²s⁻¹°C⁻¹ (refer to **Table Q5(b)**). (5 marks)
- (c) Continuous-flow heat exchangers have **THREE (3)** types of flow directions; parallel, counter and cross flows. Differentiate between counter flow and cross flow. Use diagrams to aid your answer. (10 marks)

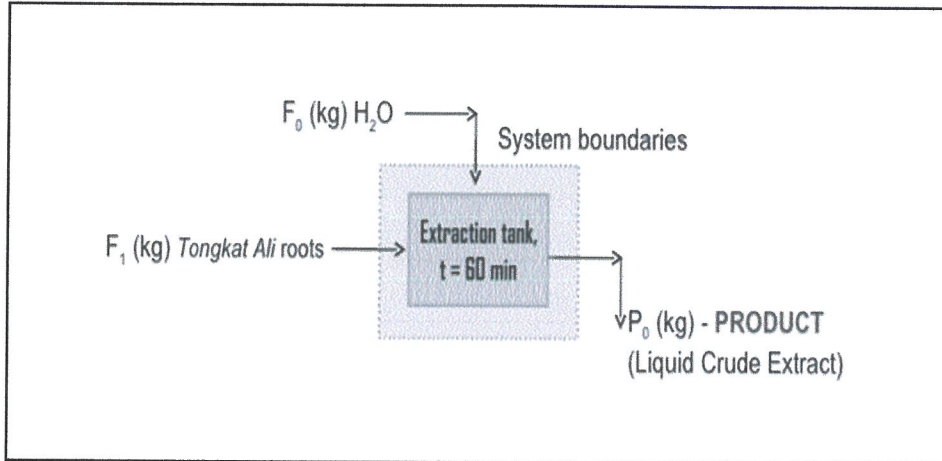
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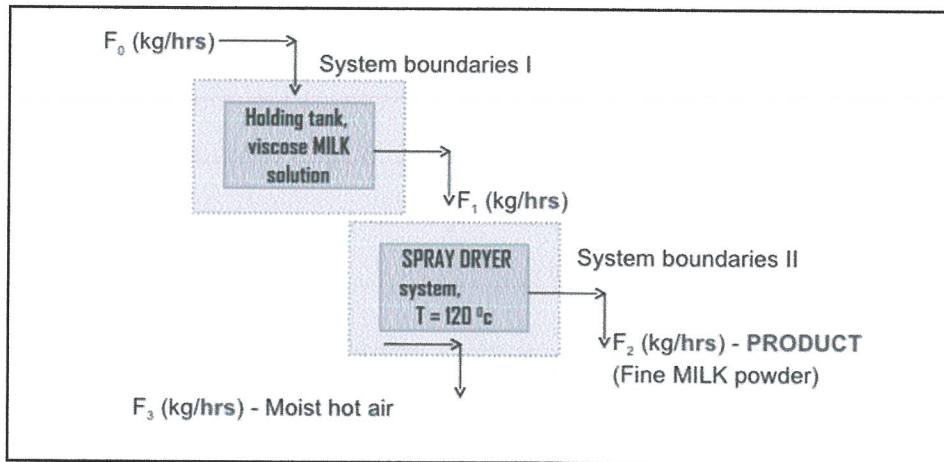
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(a)



(b)

Figure Q1: (a) Operation 1 and (b) Operation 2

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Table Q5(b): Steam Table - Saturated Steam

| Pressure Table | | | | |
|---------------------|------------------------------|---|--------------------------------------|---|
| Temperature (°C) | Pressure (Absolute) (kPa) | Enthalpy (sat. vap.) (kJkg ⁻¹) | Latent heat (kJkg ⁻¹) | Specific volume (m ³ kg ⁻¹) |
| 7.0 | 1.0 | 2514 | 2485 | 129 |
| 9.7 | 1.2 | 2519 | 2479 | 109 |
| 12.0 | 1.4 | 2523 | 2473 | 93.9 |
| 14.0 | 1.6 | 2527 | 2468 | 82.8 |
| 15.8 | 1.8 | 2531 | 2464 | 74.0 |
| 17.5 | 2.0 | 2534 | 2460 | 67.0 |
| 21.1 | 2.5 | 2540 | 2452 | 54.3 |
| 24.1 | 3.0 | 2546 | 2445 | 45.7 |
| 29.0 | 4.0 | 2554 | 2433 | 34.8 |
| 32.9 | 5.0 | 2562 | 2424 | 28.2 |
| 40.3 | 7.5 | 2575 | 2406 | 19.2 |
| 45.8 | 10.0 | 2585 | 2393 | 14.7 |
| 60.1 | 20.0 | 2610 | 2358 | 7.65 |
| 75.9 | 40.0 | 2637 | 2319 | 3.99 |
| 93.5 | 80.0 | 2666 | 2274 | 2.09 |
| 99.6 | 100 | 2676 | 2258 | 1.69 |
| 102.3 | 119 | 2680 | 2251 | 1.55 |
| 104.8 | 120 | 2684 | 2244 | 1.43 |
| 107.1 | 130 | 2687 | 2238 | 1.33 |
| 109.3 | 140 | 2690 | 2232 | 1.24 |
| 111.4 | 150 | 2694 | 2227 | 1.16 |
| 113.3 | 160 | 2696 | 2221 | 1.09 |
| 115.2 | 170 | 2699 | 2216 | 1.03 |
| 116.9 | 180 | 2702 | 2211 | 0.978 |
| 118.6 | 190 | 2704 | 2207 | 0.929 |
| 120.2 | 200 | 2707 | 2202 | 0.886 |
| 127.4 | 250 | 2717 | 2182 | 0.719 |
| 133.6 | 300 | 2725 | 2164 | 0.606 |
| 138.9 | 350 | 2732 | 2148 | 0.524 |
| 143.6 | 400 | 2739 | 2134 | 0.463 |

Note Gauge pressure \approx Absolute pressure + 100 kPa

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List of Formula

$$(\text{Pr.Gr}) = (c_p \mu / k)(L^3 \rho^2 g \beta \Delta T / \mu^2)$$

Natural convection about vertical cylinders and planes, such as vertical retorts and oven walls

$$(\text{Nu}) = 0.53(\text{Pr.Gr})^{0.25} \text{ for } 10^4 < (\text{Pr.Gr}) < 10^9, \quad h_c = 1.3(\Delta T/L)^{0.25}$$

$$(\text{Nu}) = 0.12(\text{Pr.Gr})^{0.33} \text{ for } 10^9 < (\text{Pr.Gr}) < 10^{12}, \quad h_c = 1.8(\Delta T)^{0.25}$$

Natural convection about horizontal cylinders such as a steam pipe or sausages lying on a rack

$$(\text{Nu}) = 0.54(\text{Pr.Gr})^{0.25} \text{ for laminar flow in range } 10^3 < (\text{Pr.Gr}) < 10^9$$

$$\text{for } 10^4 < (\text{Pr.Gr}) < 10^9, \quad h_c = 1.3(\Delta T/D)^{0.25}$$

$$\text{and for } 10^9 < (\text{Pr.Gr}) < 10^{12}, \quad h_c = 1.8(\Delta T)^{0.33}$$

$$A = \pi DL$$

$$\text{Heat loss rate} = h_c A (T_1 - T_2)$$

$$q = UA \Delta T_m$$

$$q = c_p G (T_1 - T_2)$$

$$\text{so } q = UA \Delta T_m = c_p G (T_1 - T_2)$$

$$= UA / \ln (\Delta T_1 / \Delta T_2) \times (T_1 - T_2)$$

but $(T_1 - T_2)$ can be written $(T_1 - T_b) - (T_2 - T_b)$,

$$\text{so } (T_1 - T_2) = (\Delta T_1 - \Delta T_2)$$

$$\text{Thus } UA \Delta T_m = UA (\Delta T_1 - \Delta T_2) / \ln (\Delta T_1 / \Delta T_2) (DT_1/DT_2)$$

$$\text{so } \Delta T_m = (\Delta T_1 - \Delta T_2) / \ln (\Delta T_1 / \Delta T_2)$$

$$q = UA \Delta T$$

$$\text{amount of steam} = q/\lambda$$



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