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**UTHM**

Universiti Tun Hussein Onn Malaysia

**UNIVERSITI TUN HUSSEIN ONN MALAYSIA**

**FINAL EXAMINATION  
SEMESTER III  
SESSION 2013/2014**

COURSE NAME : SEPARATION PROCESS  
TECHNOLOGY  
COURSE CODE : DAK 21703  
PROGRAMME : 2 DAK  
EXAMINATION DATE : AUGUST 2014  
DURATION : 3 HOURS  
INSTRUCTION : ANSWER **FOUR (4)**  
QUESTIONS ONLY

THIS QUESTION PAPER CONSISTS OF **ELEVEN (11) PAGES**

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- Q1** (a) State both solute (component B) and carrier (component A) in each example below:
- (i) Oil in a sunflower seed
  - (ii) Solid insoluble oxide containing  $\text{Na}_2\text{CO}_3$
  - (iii) Decaffeinated coffee powder (6 marks)
- (b) A feed of 5436 kg/h of a 25 wt% solution of p-dioxane in water is to be separated continuously with 4806 kg/h of benzene. The distribution coefficient,  $K'_{DB}$  is 1.35. Assuming benzene and water are mutually insoluble, determine the percentage (%) of recoveries for the following alternative procedures:
- (i) Two stage countercurrent cascade (5 marks)
  - (ii) Three stage crosscurrent cascade (5 marks)
  - (iii) If the loss due to unextracted p-dioxane is RM5/kg, calculate the loss for each procedures above (4 marks)
- (c) Sketch a solid-liquid extraction diagram complete with its four (4) streams symbolized by F, E, R, S and all its related components (A, B, and C) (5 marks)

**Q2 (a)** State the best choice of device between a trayed and a packed column for the statements below:

- (i) Column diameter is less than 2 ft
- (ii) Column height is less than 20 ft and low pressure drop
- (iii) Pressure drop above 200 psia and low liquid velocities
- (iv) High degree of separation required

(8 marks)

(b) A feed gas to an absorber containing 17 mol% CO<sub>2</sub> and 83 mol% air, is to be absorbed in a 5.0-N solution of triethanolamine (or amine), containing 0.04 mol CO<sub>2</sub> per mole of amine solution. The column operates isothermally at 25°C, and the exit liquid contains 87.4% of the CO<sub>2</sub> in the feed gas to the absorber, and if absorption is carried out in a six (6) theoretical plate column, use equilibrium data below to:

**Table Q2 (b)**

Equilibrium Data						
<b>X</b>	0.003	0.008	0.015	0.023	0.032	0.043
<b>Y</b>	0.01	0.02	0.03	0.04	0.05	0.06
Equilibrium Data						
<b>X</b>	0.055	0.068	0.083	0.099	0.12	
<b>Y</b>	0.07	0.08	0.09	0.10	0.11	

- (i) State the value of X<sub>0</sub>, Y<sub>N+1</sub>, and Y<sub>1</sub> (3 marks)
- (ii) Calculate the exit gas (top product) composition in terms of mol% (4 marks)
- (iii) Plot the equilibrium curve of Y versus X (4 marks)
- (iv) Determine the value of X<sub>N</sub> from trial and error method, using the value of Y<sub>N+1</sub> (3 marks)
- (v) Determine the moles of amine per mole of feed gas (3 marks)

**Q3** A stream feed of five hundred and forty lbmol/h of a mixture of 60 mol% benzene (LK-component x) and 40 mol% toluene (HK-component y) is to be separated to produce a liquid distillate and a liquid bottoms product of 90 mol% and 10 mol% benzene respectively. The feed enters the column at 1 atm with a molar percent vaporization equal to the distillate-to-feed ratio. Use the McCabe-Thiele method to compute:

- (a) Minimum equilibrium stages,  $N_{\min}$  using **Figure Q3 (a)** (7 marks)
- (b) Minimum reflux ratio,  $R_{\min}$  (8 marks)
- (c) Number of equilibrium stages,  $N$  given that the reflux ratio,  $R = 1.4R_{\min}$  using **Figure Q3 (b)** (8 marks)
- (d) The optimum feed-stage location based on the answer in Q3 (c) (2 marks)

- Q4** (a) State the use of each equation below:
- (i) Fenske equation (state one use only)
  - (ii) Underwood equations
  - (iii) Gilliland correlation
  - (iv) Kirkbide equation (8 marks)
- (b) A debutanizer as shown in **Figure Q4 (b)** is operated at a uniform operating pressure of 80 psia throughout the column. The distillate (top) temperature is 123°F and its bottoms temperature is 340°F.
- (i) Determine the two key components (i, j) (2 marks)
  - (ii) Tabulate the mole fraction for all components in distillate ( $x_D$ ), and mole fraction for all components in bottoms ( $x_B$ ) (4 marks)
  - (iii) Calculate the relative volatility,  $\alpha$  for component i and j,  $\alpha_m$  using equilibrium data in **Table Q4 (b)** (note that LK = i and HK = j) (6 marks)
  - (iv) Estimate the minimum theoretical stages,  $N_{min}$  by Fenske equation (3 marks)
  - (v) Determine the actual number of stages, N if its value is 2 times  $N_{min}$  (2 marks)

**Q5** A simple batch pot is used to separate methanol ( $\text{CH}_3\text{OH}$ ) from water using batch distillation method. The pot is initially filled with  $W_0 = 50$  moles of an 80 mol% methanol at atmospheric pressure of 1 atm. The solution is then distilled to obtain the desired distilled concentration ( $x_D$ ) of 89.15% of methanol. Using trial and error from **Figure Q5 (a)** and **Figure Q5 (b)**, estimate at which value of  $D_{Total}$ ,  $W_{final}$  and  $x_{W final}$  yield the value of  $x_D \approx 89.15\%$  when:

(a) The first guessed value of  $x_{W final} = 0.60$  (8 marks)

(b) The second guessed value of  $x_{W final} = 0.65$  (8 marks)

(c) A tabulated data of vapor pressure,  $P^s$  for a vapor-liquid mixture of water ( $\text{H}_2\text{O}$ ) and methane ( $\text{CH}_4$ ) at  $P = 2$  atm and  $T = 20$  and  $80^\circ\text{C}$  is as below:

T ( $^\circ\text{C}$ )	$P^s$ for $\text{H}_2\text{O}$ (atm)	$P^s$ for $\text{CH}_4$ (atm)
20	0.02307	$3.76 \times 10^4$
80	0.4673	$6.82 \times 10^4$

(i) Calculate the K-value and  $\alpha$  for water over methane at  $20^\circ\text{C}$  (3 marks)

(ii) Calculate the K-value and  $\alpha$  for water over methane at  $80^\circ\text{C}$  (3 marks)

(iii) Sketch a simple batch distillation (or Rayleigh distillation) (3 marks)



- Q6** (a) State four (4) points to compare an absorber with a stripper with the aid of suitable diagrams (10 marks)
- (b) For a stream of liquid comprising of component A and B:
- (i) Express the relative volatility of A to B,  $\alpha_{A,B}$  in terms of  $P^s$  and P
  - (ii) Express the relative volatility of A to B,  $\alpha_{A,B}$  in terms of  $\gamma$ ,  $P^s$  and P
  - (iii) Given that  $K = 0.55$ , rearrange the K-value equation so that Y is in the left side of the equation
  - (iv) Given that  $K = 0.45$ , rearrange the K-value equation so that X is in the left side of the equation (12 marks)
- (c) State three (3) parameters that can be determined from the McCabe-Thiele Method (3 marks)

- END OF QUESTION -

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### LIST OF FORMULA

$$E = K'_{DB} S / F_A$$

$$K'_{DB} = Y_B / X_B$$

$$1 - X_B^{(n)} / X_B^{(F)} = 1 - 1 / (1 + E/N)^n$$

$$1 - X_B^{(R)} / X_B^{(F)} = 1 - 1 / (1 + E + E^N)$$

$$1 - X_B^{(R)} / X_B^{(F)} = Y_1 (S - R F_A) / F_B$$

$$Y_{N+1} = X_N (L' / V') + Y_1 - X_0 (L' / V')$$

$$Y_{N+1} = \text{mol B in} / \text{mol gas (A)}$$

$$Y_1 = \text{mol B out} / \text{mol gas (A)}$$

$$X_N = \text{mol B out} / \text{mol liq solvent (C)}$$

$$X_0 = \text{mol B in} / \text{mol liq solvent (C)}$$

$$y = Y / (1 + Y)$$

$$z_F (F) = x_D (D) + x_B (B)$$

$$F = D + B$$

$$q = 1 - (D/F)$$

$$\text{Absorber's slope operating line} = L' / V'$$

$$\text{McCabe Thiele's slope rectifying operating line} = (R / R + 1)$$

$$\text{McCabe Thiele's slope rectifying operating line (min reflux)} = (R_{\min} / R_{\min} + 1)$$

$$\text{McCabe Thiele's slope q-line} = (q / q - 1)$$

$$\text{normal slope, } m = \Delta y / \Delta x$$

$$\alpha_m = [(\alpha_{ij})_N \times (\alpha_{ij})_1]^{0.5}$$

$$N_{\min} = \log [(x_{Di} / x_{Dj}) (x_{Bi} / x_{Bj})] \div \log \alpha_m$$

$$\alpha_{i,j} = \frac{K_i}{K_j} \text{ or } \alpha_{A,B} = \frac{K_A}{K_B}$$

$$W_{final} = W_0 \exp\left(-\int_{x_0}^x \frac{dx}{y-x}\right) \text{ or } W_{final} = W_0 \exp(-\text{Area under the curve})$$

$$D_{total} = W_0 - W_{final}$$

$$x_D = \frac{W_0 x_0 - W_{final} x_{W final}}{D_{total}}$$

$$K_n = \frac{y_n}{x_n} = \frac{Y_n / (1 + Y_n)}{X_n / (1 + X_n)}$$

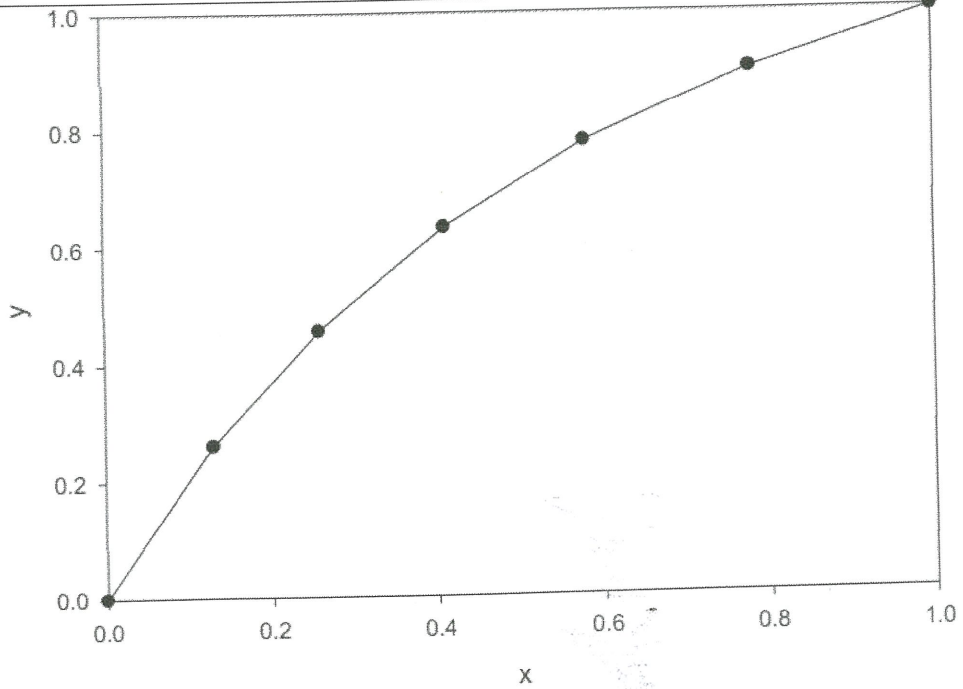
$$K = \frac{P^s}{P} \text{ or } K = \frac{\gamma P^s}{P}$$



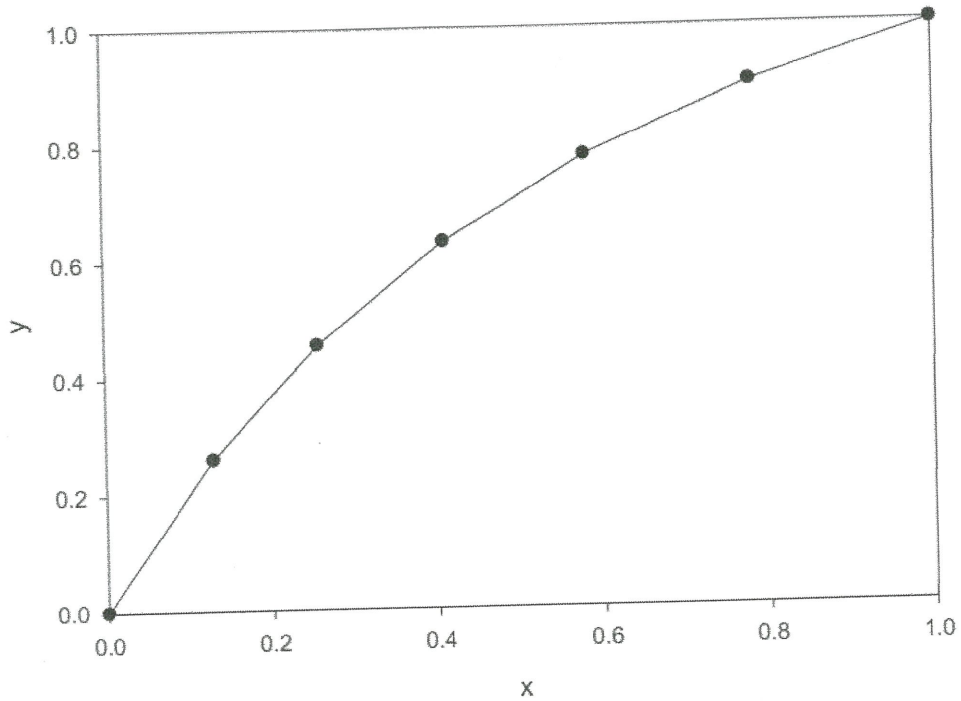
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**FIGURE Q3 (a)**

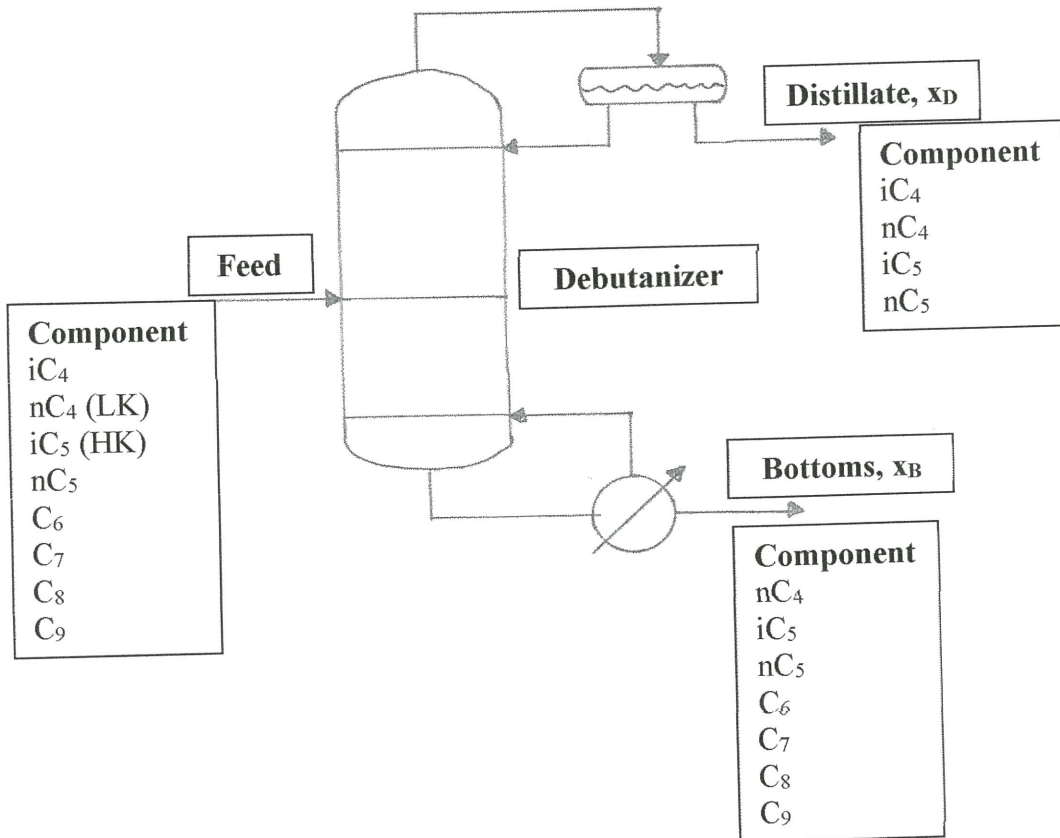


**FIGURE Q3 (b)**

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**FIGURE Q4 (b)**

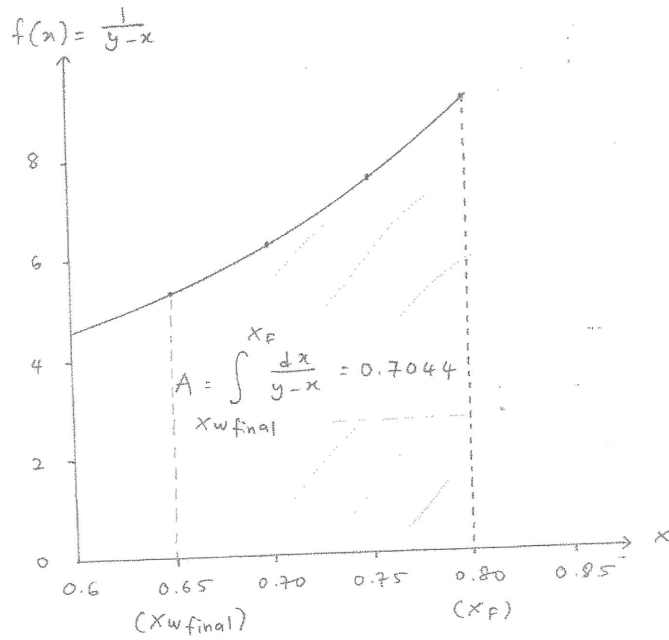
**TABLE Q4 (b)**

Component	Distillate, D (lbmol/h)	Bottoms, B (lbmol/h)	K-value at 123°F (top, N)	K-value at 340°F (bottom, I)
iC <sub>4</sub>	12	~0	1.04 0.496	5.21 3.61
nC <sub>4</sub> (LK)	450	6		
iC <sub>5</sub> (HK)	13	23		
nC <sub>5</sub>	2	14		
C <sub>6</sub>	~0	23		
C <sub>7</sub>	~0	39		
C <sub>8</sub>	~0	272		
C <sub>9</sub>	~0	31		
	477	408		

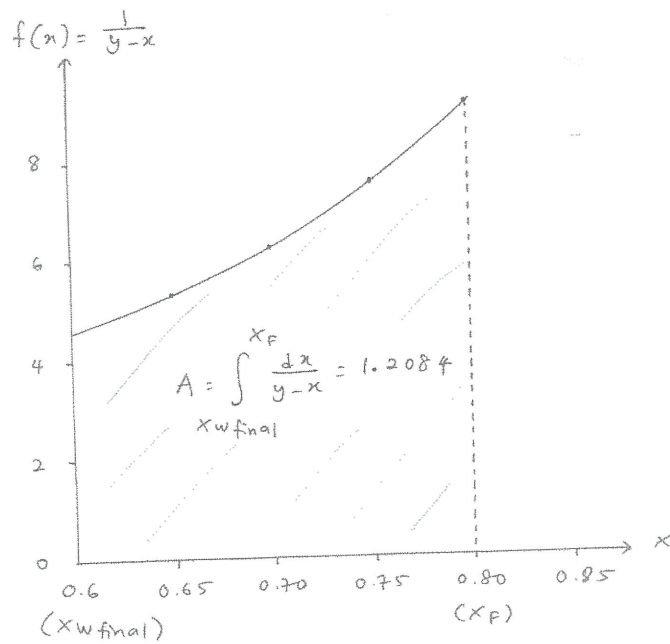
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**FIGURE Q5 (a)**



**FIGURE Q5 (b)**